

Micropile Threaded Connections at PDX Airport TCORE

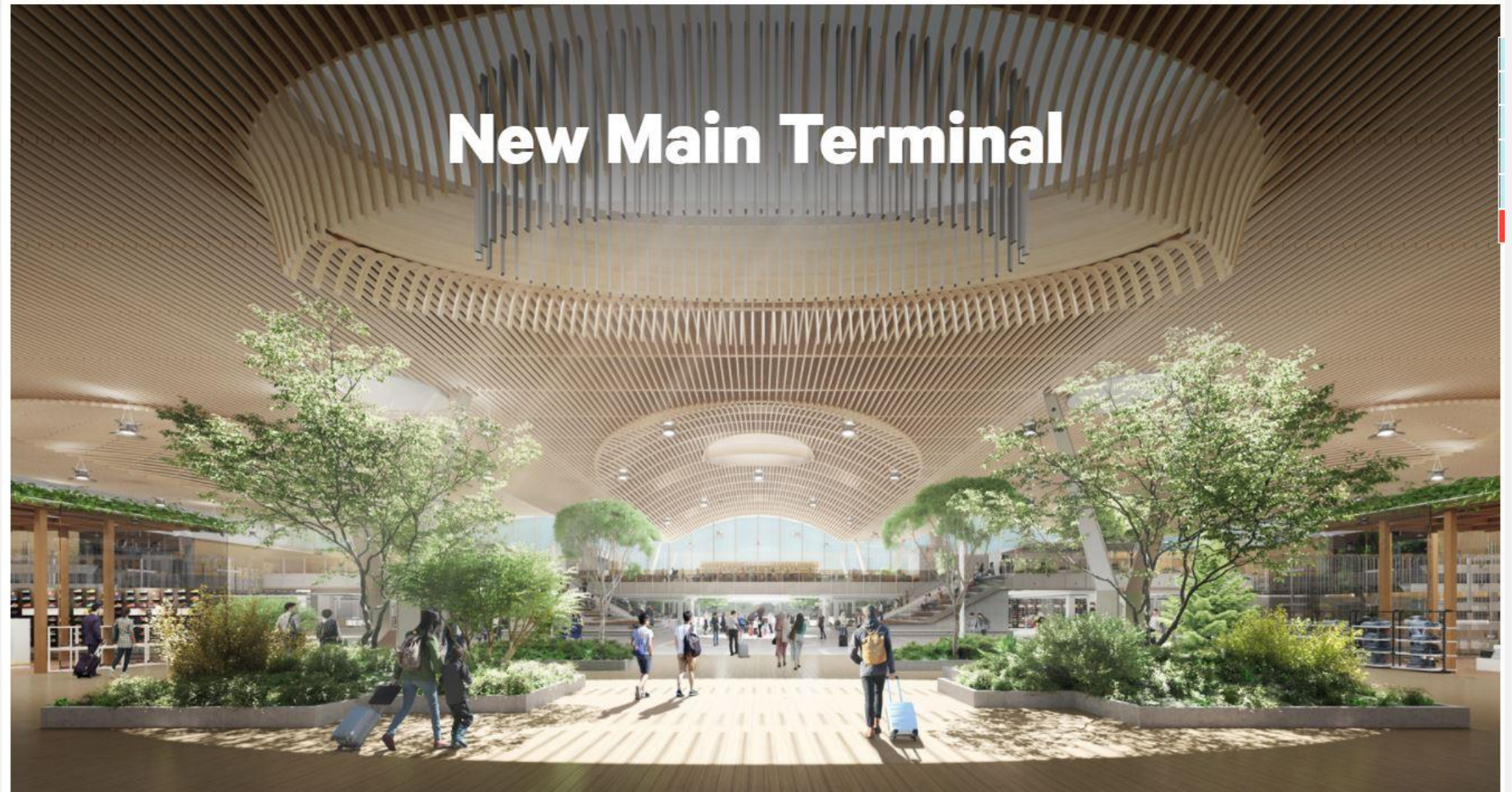


CONDON · JOHNSON
& ASSOCIATES, INC.

CONTRACTORS AND ENGINEERS

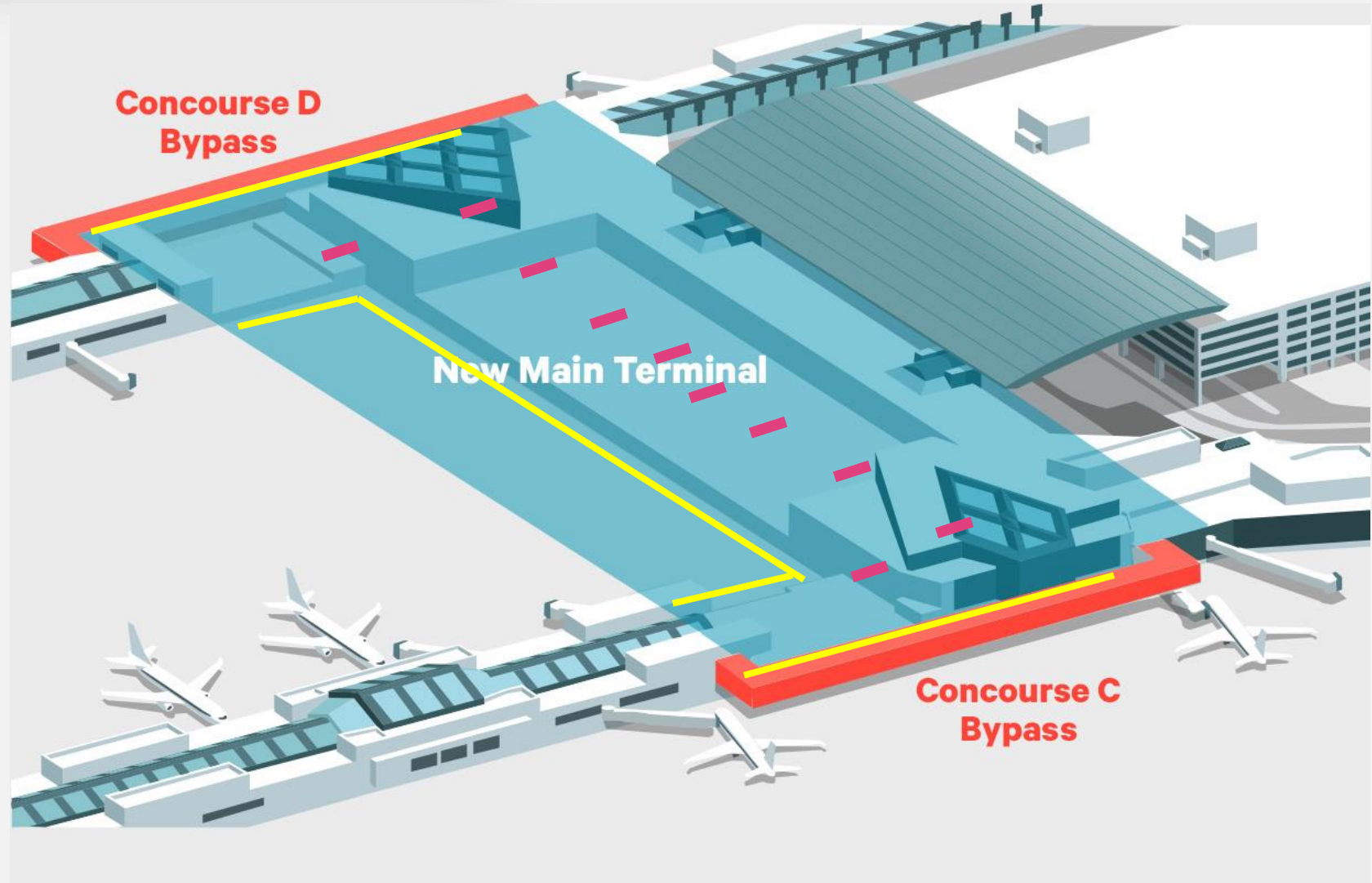
PDX TCORE WESTERN EXPANSION

- Overall Project is \$1B renovation and expansion of the PDX Main Terminal
- Owner Port of Portland
- GC Hoffman-Skanska JV



PDX T CORE WESTERN EXPANSION

- 750ea total quantity
- Unlimited Overhead Piles, 433ea
- Limited Overhead Piles, 315ea
- Micropiles - Design Build Criteria
- 9-5/8" 300kip Service Compression
- Minimum 100-ft Cased Length due to liquefaction



PDX TCOE WESTERN EXPANSION



CAUSE FOR BEND TESTING

- Once the structural design & liquefaction analysis was fully completed, Owner's engineers required micropiles to have 1,600 kip-in of moment capacity in the top 40' of the micropile.
- City of Portland (Permitting Agency) was not comfortable using the 50% moment capacity design philosophy despite showing former full scale testing.
- CJA proposed doing a series of bend testing on varying casing sizes to see what was the optimal diameter x thickness to meet 1,600 k-in

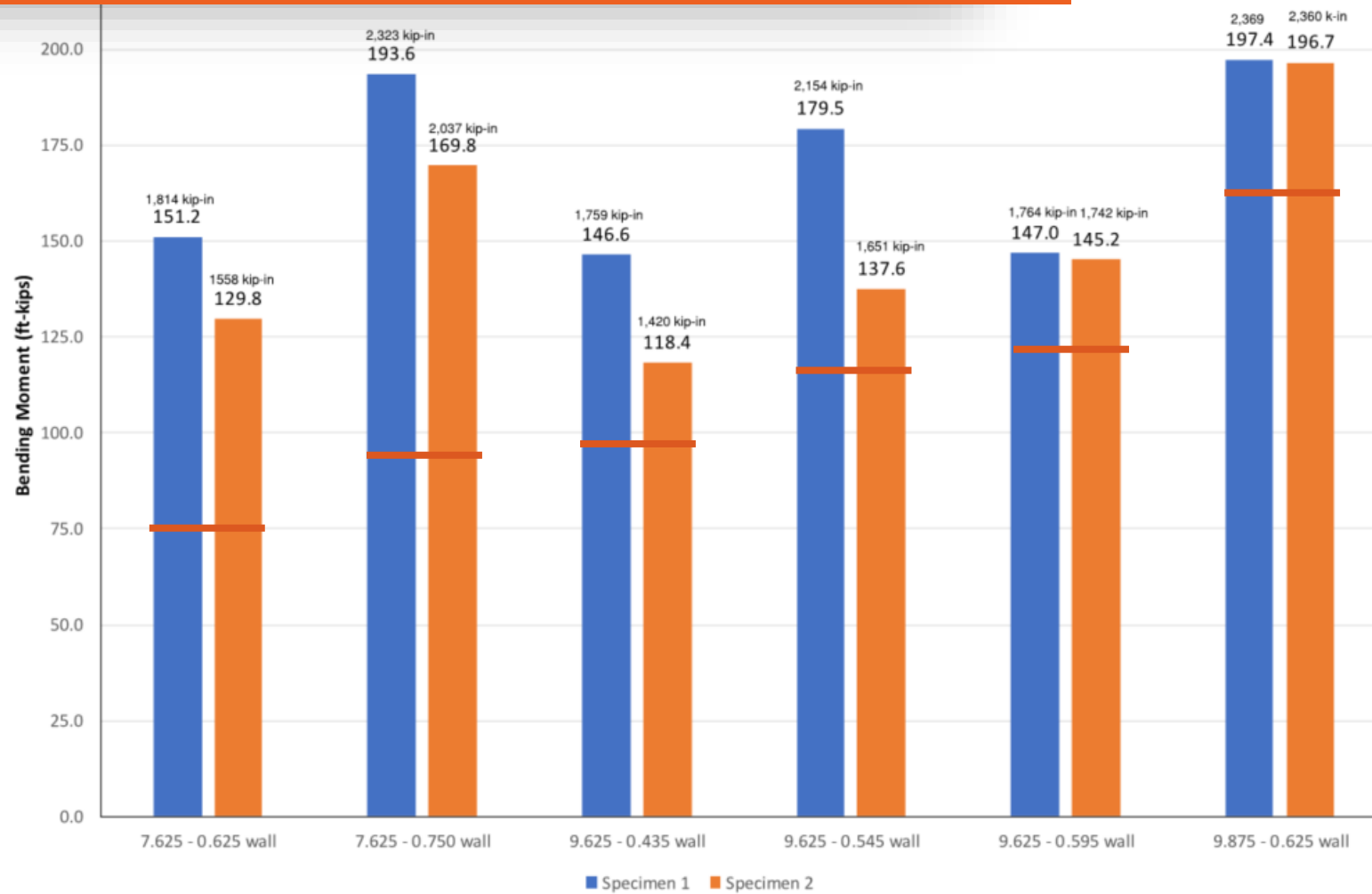


Casing Bend Testing

- Objective of testing was to gather project specific information for Permit Approval with City of Portland
- Four point bend test performed by Stress Engineering in Houston, Texas
- All casing was from OCI Division
- Thread Length was 2.5" from shoulder to shoulder for all joints.
- Uses a tapered thread which has a thickened section towards the shoulder



1st Round of Bend Testing



1st Round of Bend Testing

| CASING | OD | WALL THICKNESS | THOERETICAL YIELD STRENGTH (KSI) | UNREDUCED CASING SECTION (BLANK) BENDING CAPACITY (K-IN) | MEASURED JOINT BENDING CAPACITY (K-IN) | ACTUAL % |
|-----------------|-------|----------------|----------------------------------|----------------------------------------------------------|----------------------------------------|----------|
| 7-5/8" X 0.625" | 7.625 | 0.625 | 80 | 1780.58 | 1686 | 95% |
| 7-5/8" X 0.75" | 7.625 | 0.750 | 80 | 2032.16 | 2180.4 | 107% |
| 9-5/8" x 0.435 | 9.625 | 0.435 | 80 | 2208.96 | 1590 | 72% |
| 9-5/8" X 0.545" | 9.625 | 0.545 | 80 | 2672.98 | 1903.2 | 71% |
| 9-5/8" X 0.595 | 9.625 | 0.595 | 80 | 2872.37 | 1753.2 | 61% |
| 9-7/8" x 0.625" | 9.875 | 0.625 | 100 | 3952.18 | 2365.2 | 60% |

- Average of 2ea bend tests per joint size.
- All test specimens were grout filled with NO center bar.

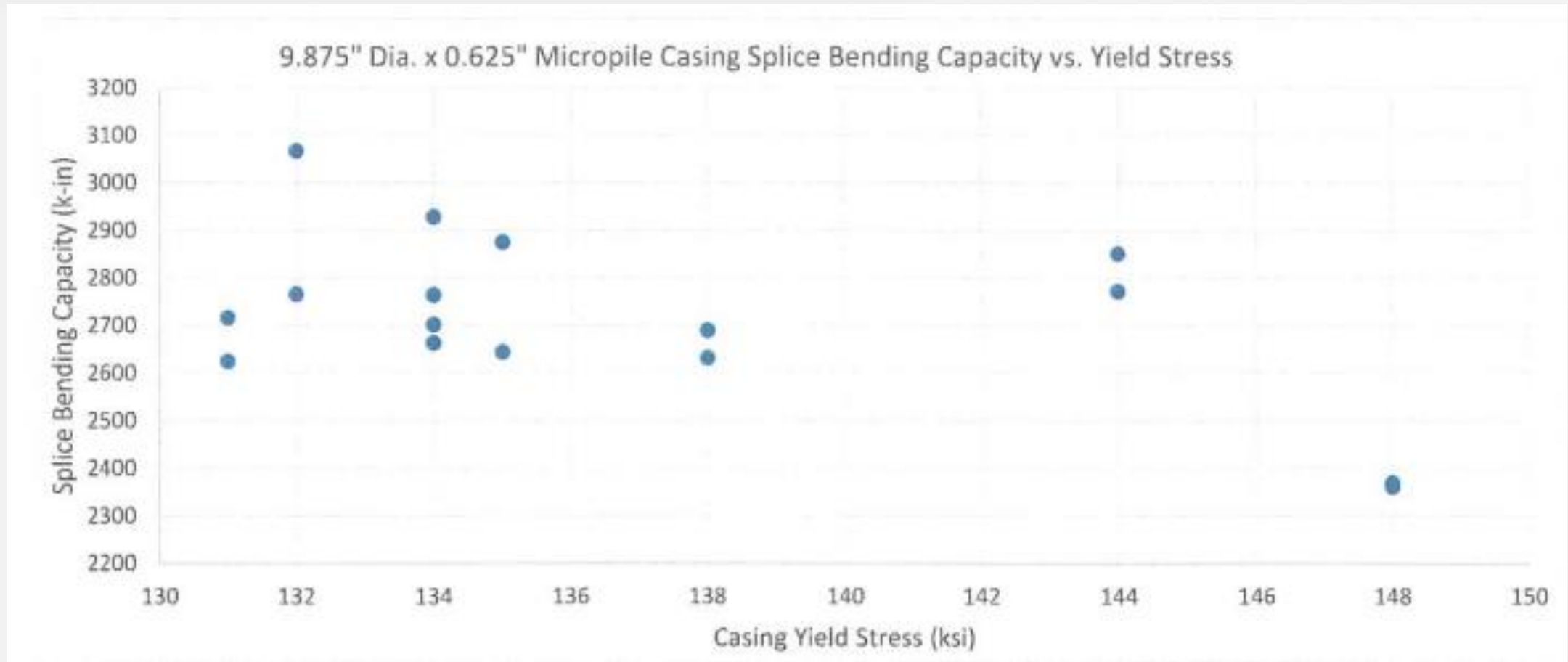


2nd Round of Bend Testing

- Owner opted for the 9-7/8" x 0.625" to be conservative but determined additional testing was required to develop a sample size that would be make it through permitting.
- Casing supplier could potentially provide casing with a 100KSI yield strength, however the lowest yield test specimen was 130KSI.
- This lead us down a rabbit hole of what if we had a load of casing delivered to the site that had a yield less 130 KSI.
- 16ea additional 9-7/8" x 0.625" bend tests were completed to see if we could develop a correlation between yield and bending capacity



2nd Round of Bend Testing



2nd Round of Bend Testing

| Casing | Specimen | Measured Bending Capacity (Kip-ft) | Kip-In | % of Unreduced Bending Section | Coupon Yield Stress (KSI) |
|-----------------|----------|------------------------------------|--------|--------------------------------|---------------------------|
| 9.875" x 0.625" | 1A | 225.1 | 2701.2 | 68% | 134 |
| 9.875" x 0.625" | 2A | 244 | 2928 | 74% | 134 |
| 9.875" x 0.625" | 1B | 230.4 | 2764.8 | 70% | 132 |
| 9.875" x 0.625" | 2B | 255.5 | 3066 | 78% | 132 |
| 9.875" x 0.625" | 1D | 224.1 | 2689.2 | 68% | 138 |
| 9.875" x 0.625" | 2D | 219.3 | 2631.6 | 67% | 138 |
| 9.875" x 0.625" | 1F | 220.3 | 2643.6 | 67% | 135 |
| 9.875" x 0.625" | 2F | 223.9 | 2686.8 | 68% | 135 |
| 9.875" x 0.625" | 1R | 221.9 | 2662.8 | 67% | 134 |
| 9.875" x 0.625" | 2R | 230.3 | 2763.6 | 70% | 134 |
| 9.875" x 0.625" | 1S | 226.3 | 2715.6 | 69% | 131 |
| 9.875" x 0.625" | 2S | 218.7 | 2624.4 | 66% | 131 |
| 9.875" x 0.625" | 1B2 | 230.9 | 2770.8 | 70% | 144 |
| 9.875" x 0.625" | 2B2 | 237.5 | 2850 | 72% | 144 |
| 9.875" x 0.625" | DD-1 | 192.5 | 2310 | 58% | 148 |
| 9.875" x 0.625" | DD-2 | 202.4 | 2428.8 | 61% | 148 |
| 9.875" x 0.625" | FF-1 | 194 | 2328 | 59% | 113 |
| 9.875" x 0.625" | FF-2 | 196.9 | 2362.8 | 60% | 113 |
| | | | | 67% | |



Predominate Failure Method

Specimen - 9.875" OD - 0.625" Wall - S1



Predominant Failure Mode - Thread Jumpout



Single Pin Critical Failure

Specimen - 9.625" OD - 0.435" Wall - S2



Predominant Failure Mode - Critical Cross-Section Failure



Conclusions

- All joint testing achieved 50% bending capacity of the unreduced section
- No significant correlation between yield strength of material and bending capacity.
- Failure mode was almost exclusively thread jump out
- Smaller Diameter and Thicker casing resulting in higher bending %



Questions?

