

International Workshop on Micropiles
Washington, D.C.
22 – 25 September 2010



UTILIZATION OF MICROPILES FOR HEAT EXCHANGE

By

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Lizzi Scholarship Recipient
2010



What this presentation is about?

- Introduction
- Micropiles and Geothermal Energy
- Challenges of Energy Micropiles
- Virginia Tech on the road
- What is next?
- Summary



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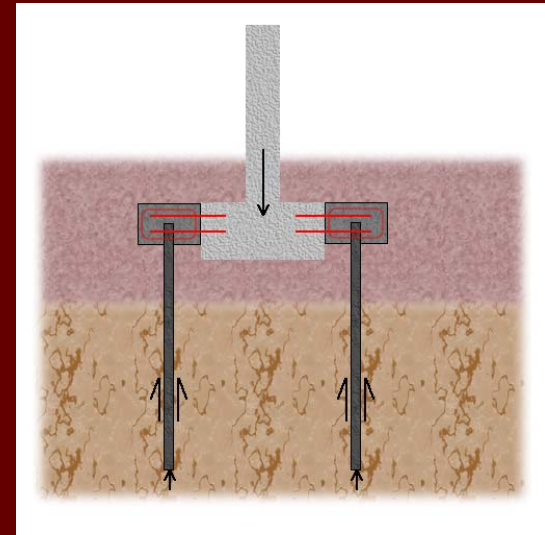


Outline

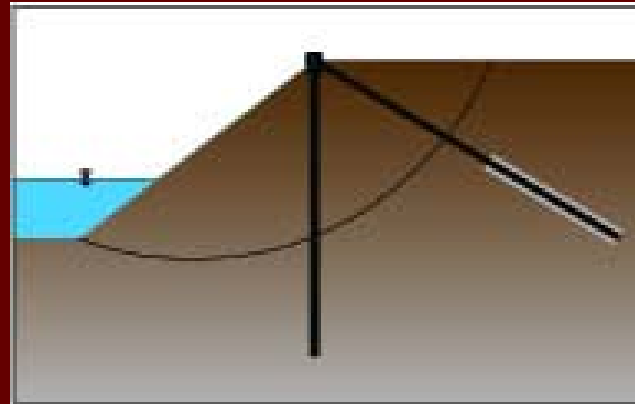
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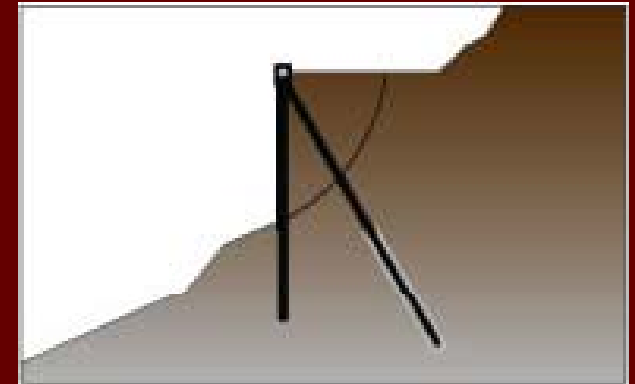
Replace deep foundations



Underpinning



Slope Stability



Side Support & Earth Retention



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Micropiles as Heat Exchangers

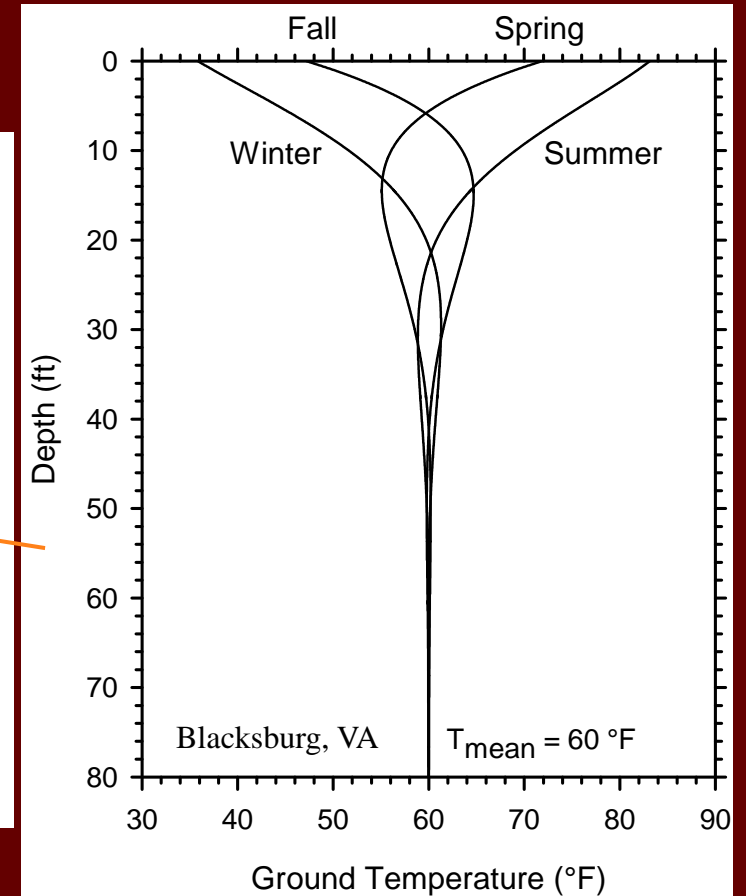
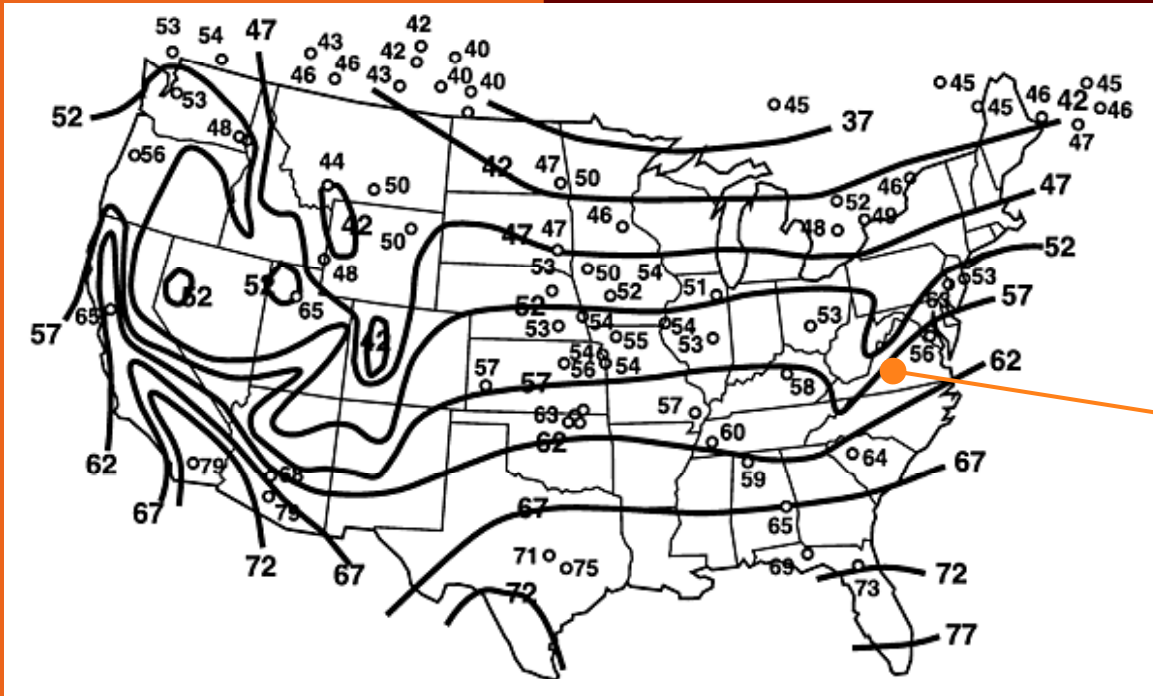


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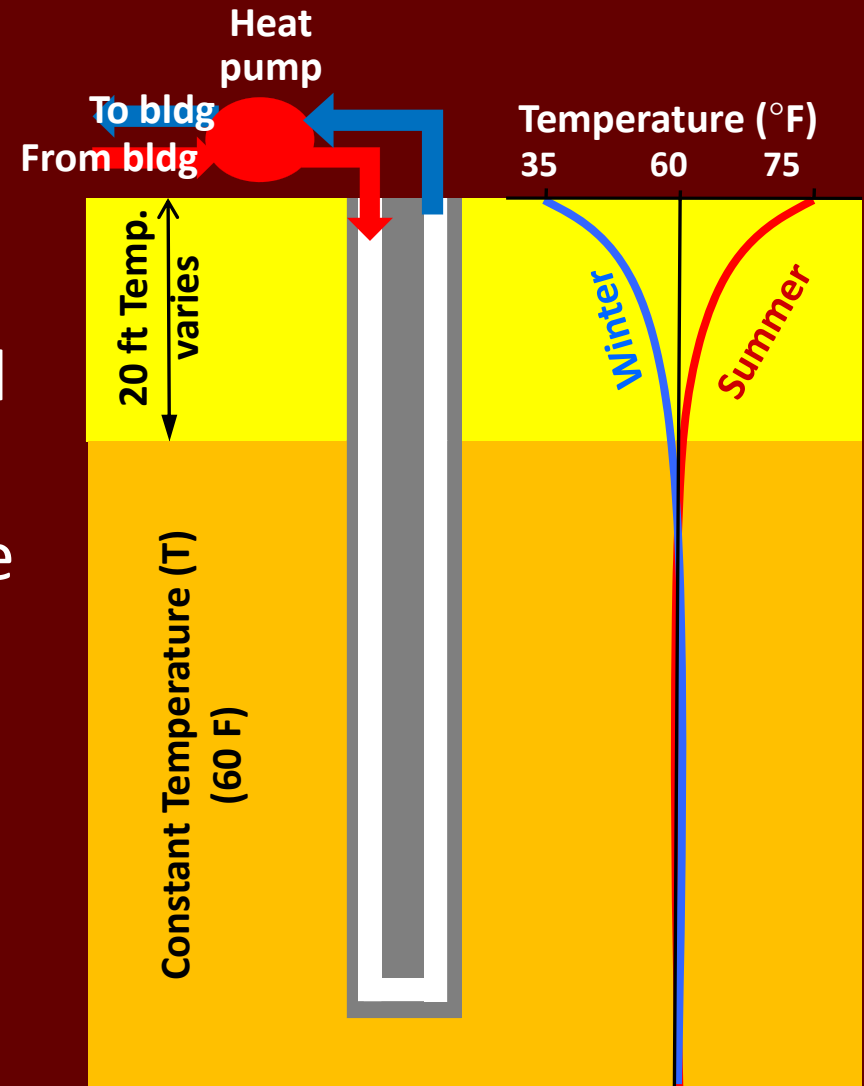
- What is next?

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Micropiles for Energy Utilization

- circulation tubes
- Heat pump
- Geothermal fluid (water & antifreeze mix.)



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 VirginiaTech
Invent the Future

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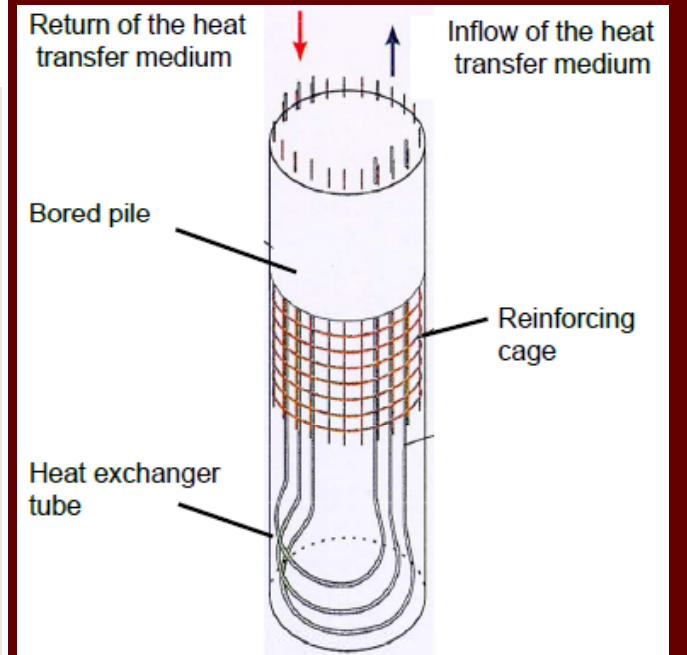
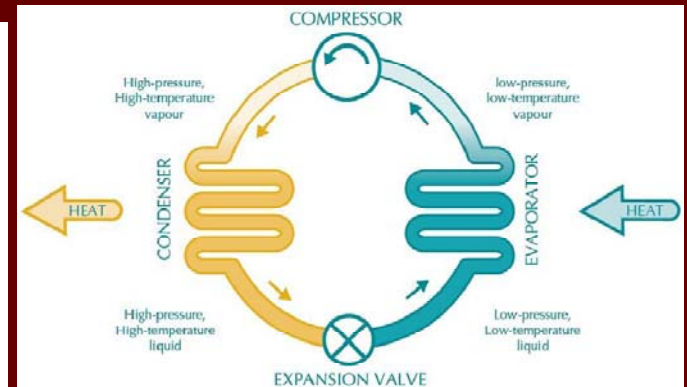
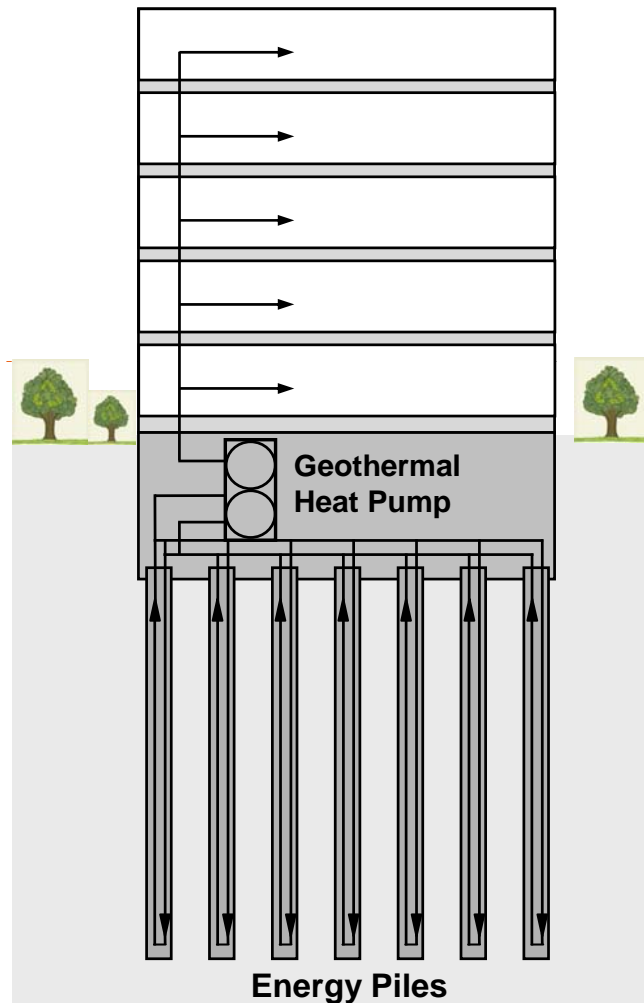
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Micropiles for Energy Utilization

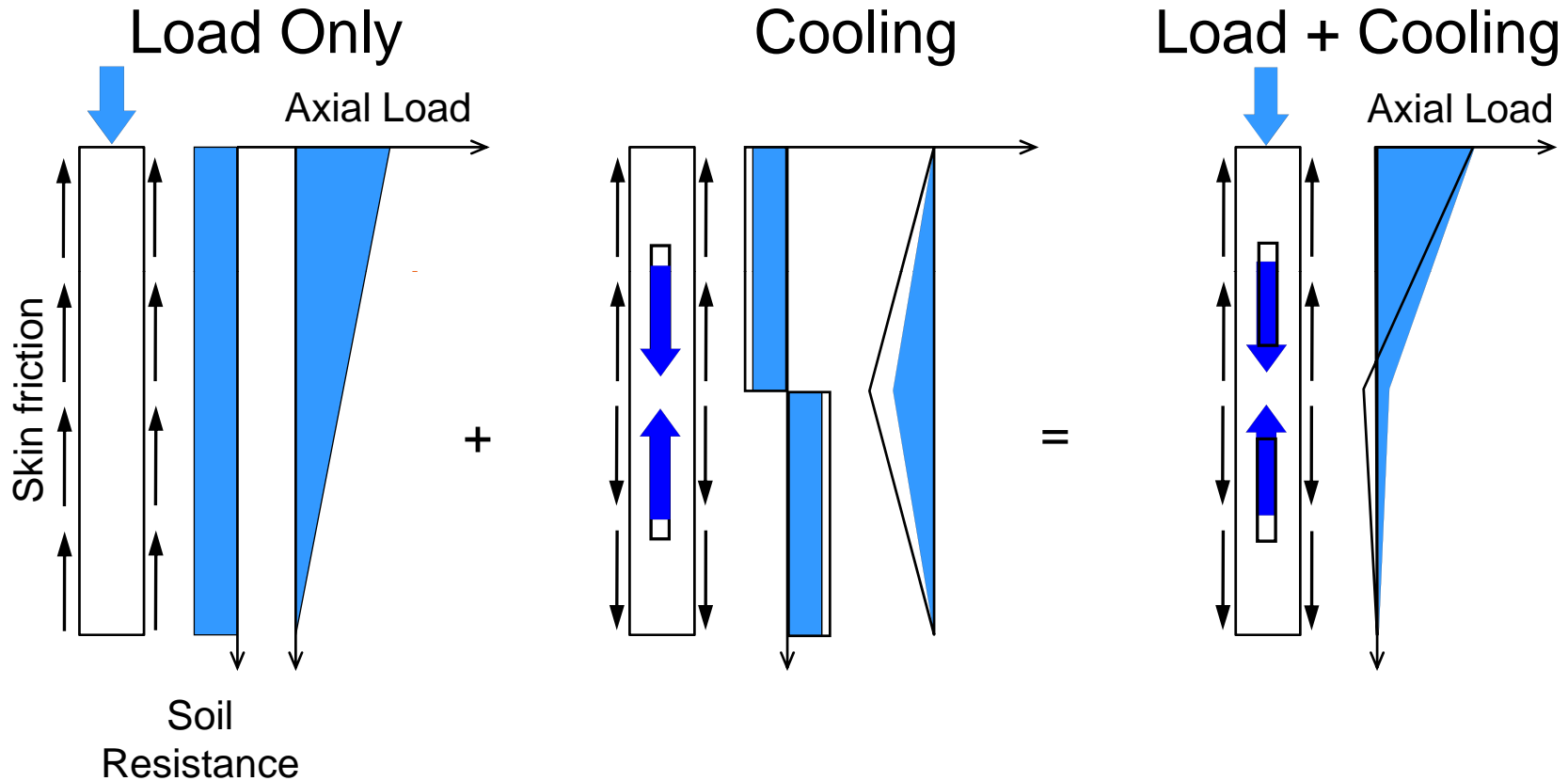
Air conditioning (heating and cooling)



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Challenges for the use of Micropiles as GHEX



Load carrying mechanism



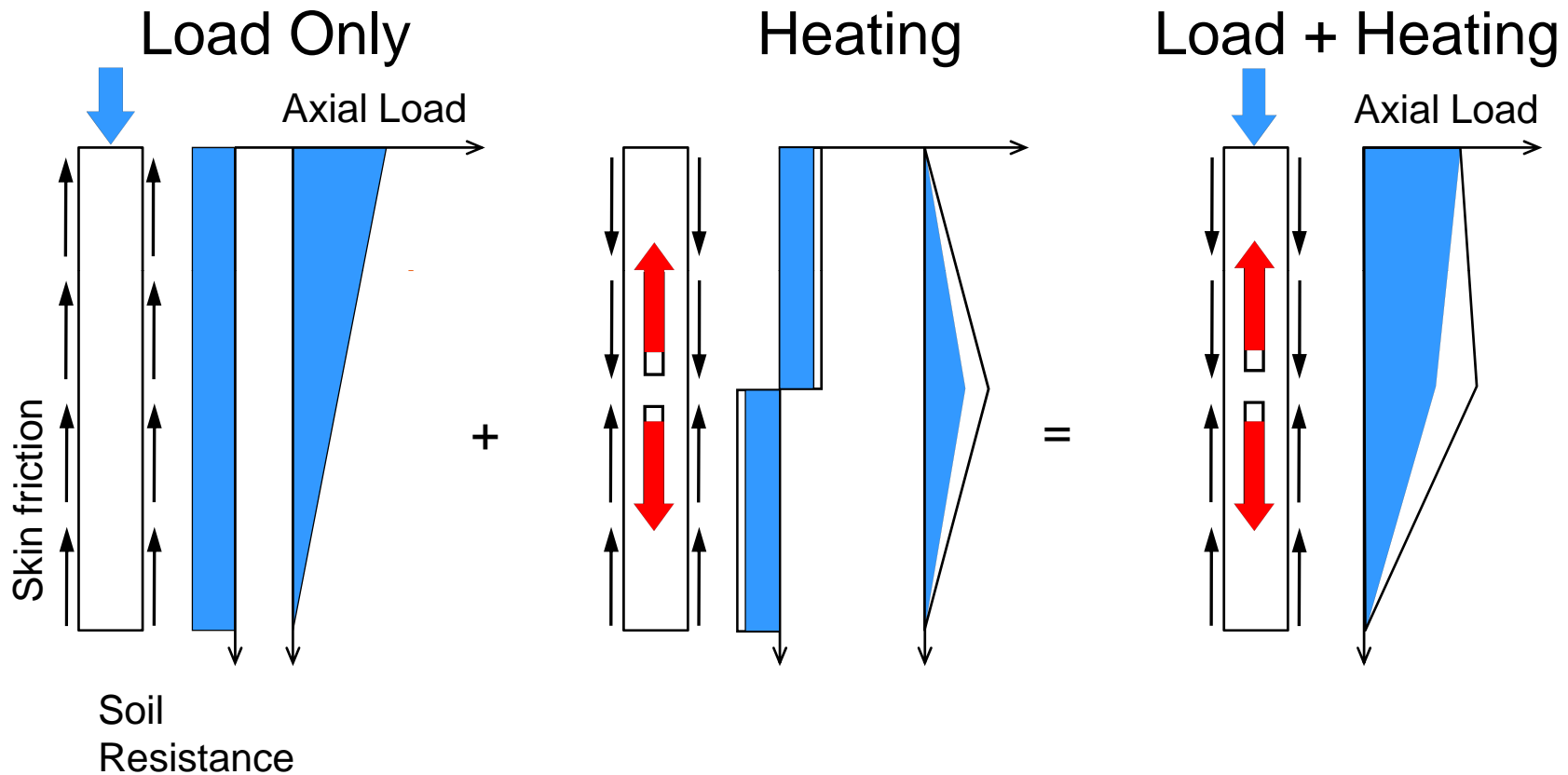
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Load carrying mechanism



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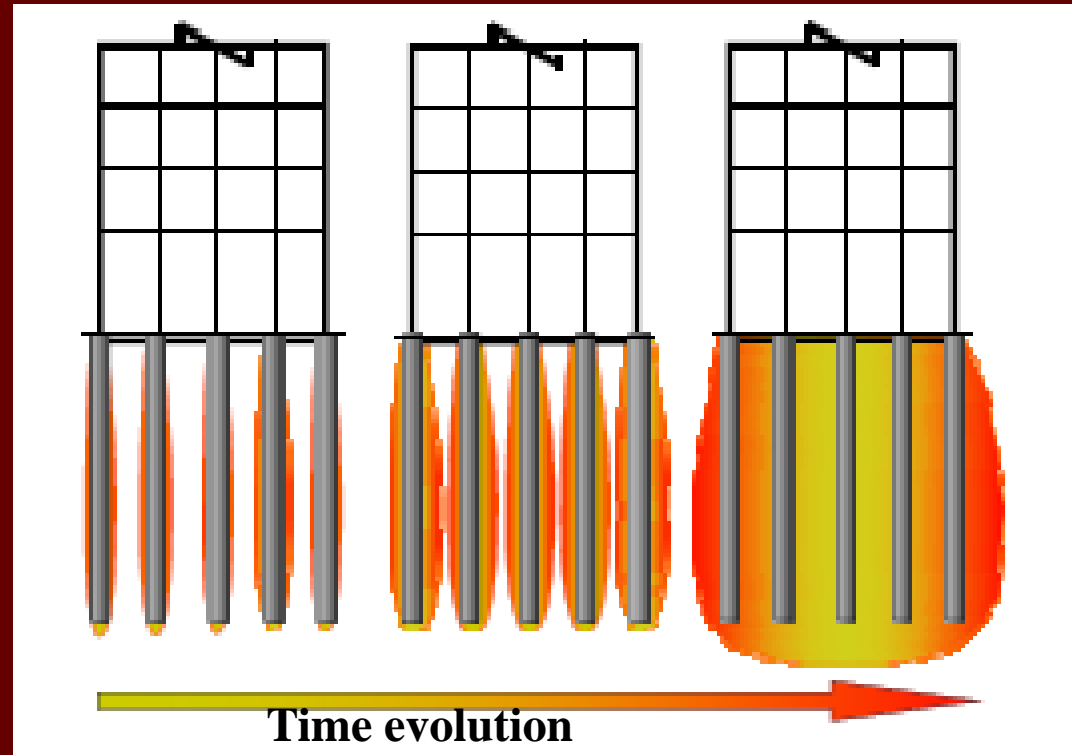


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Challenges for the use of Micropiles as GHEX

- Long term thermal cycle loading effects



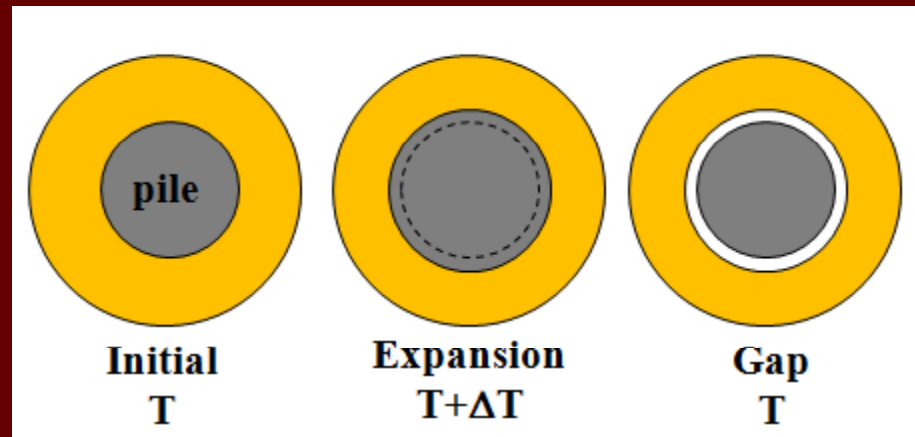
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Challenges for the use of Micropiles as GHEX

- Overall thermo-mechanical response in short-term as well as long term



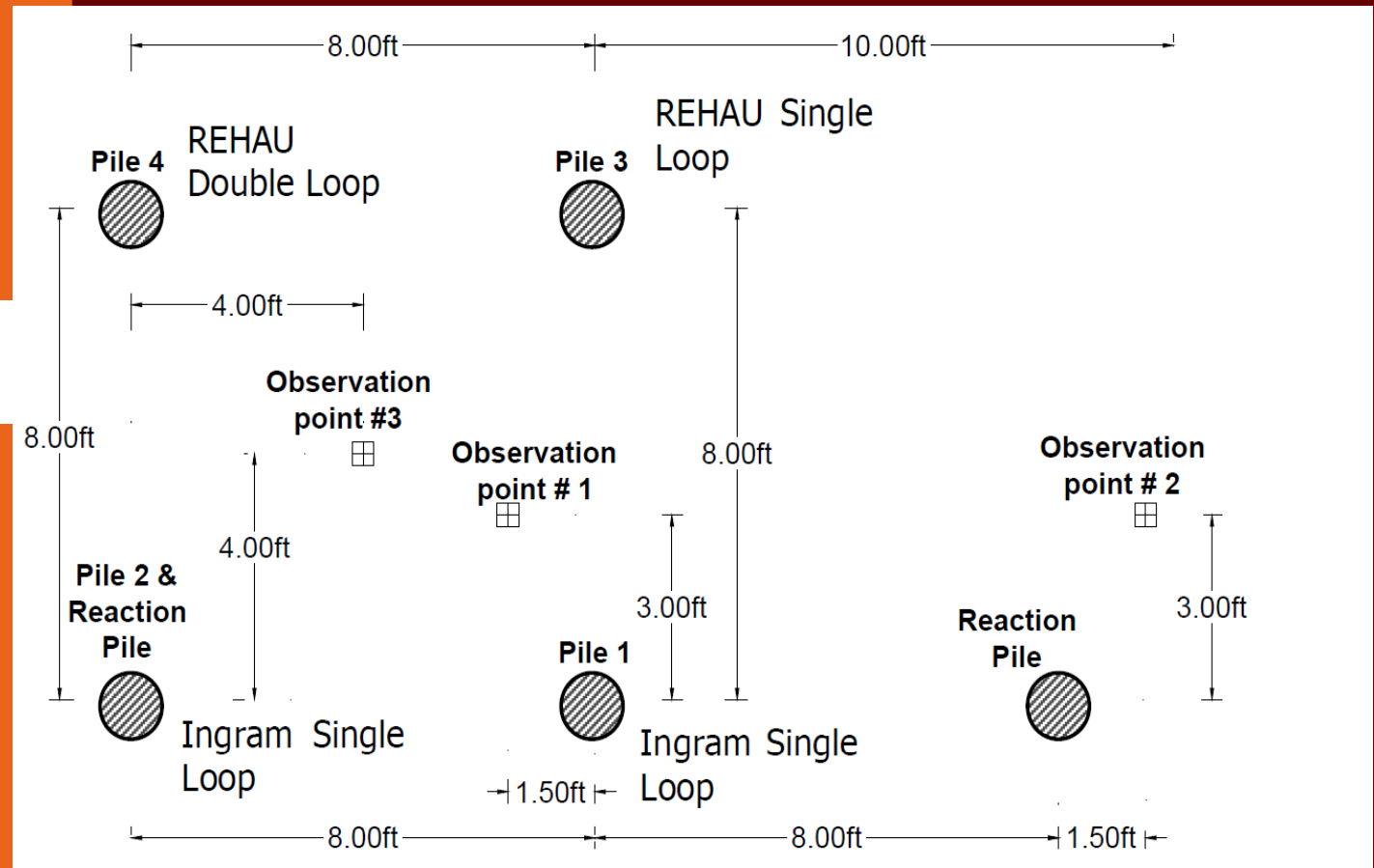
- Group effect under thermo-mechanical loads!!!!

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Virginia Tech Field Test



- Different tubes, tube configurations.



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Micropiles for Energy Utilization

- Virginia Tech Micro-pile Construction



Drilling



Installing Tubes

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Pressure test



Instrumentations

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Grouting



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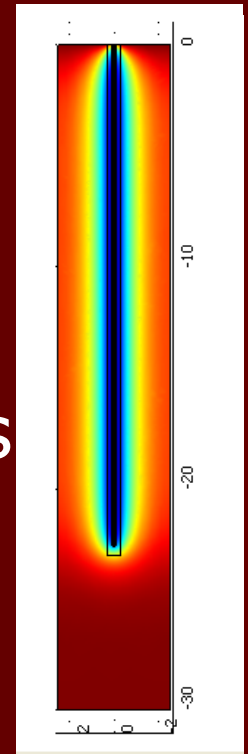
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What is Next?

- Running field test
 - Thermal test
 - Thermo-mechanical test
- Numerical modeling and use of the field data for calibration purposes
- Generalization the results
 - Other field tests,
 - Laboratory thermo-mechanical tests on different soils



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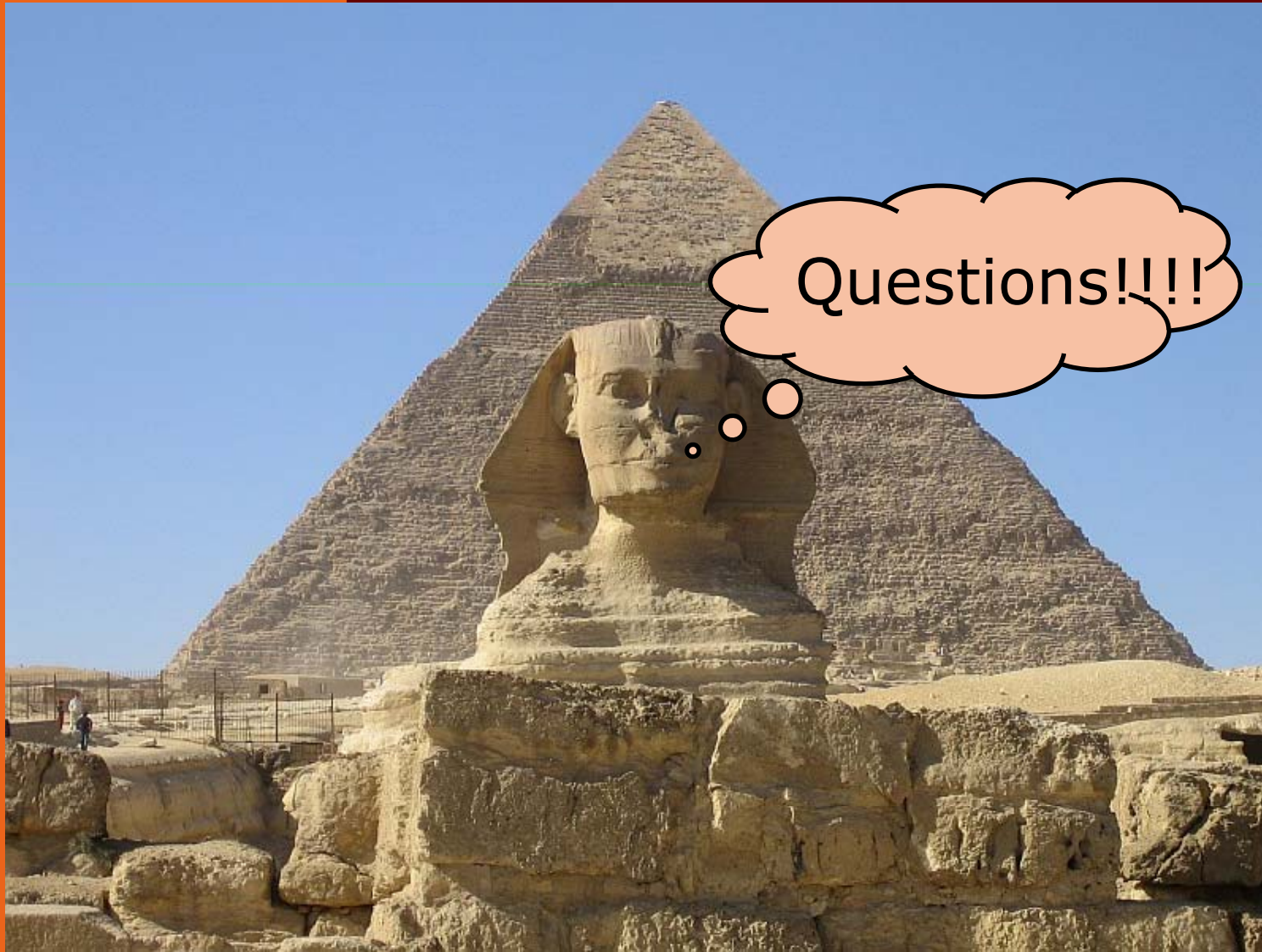
Summary

- Micropiles are being used for different purposes, why not Geothermal?
- Different challenges need to be addressed and studied
- Field tests are the best way to investigate things to be built in-situ
- Results will be available once field test is performed.



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Required GHEX Length (L)

$$L = \frac{G C_p (T_{source, in} - T_{source, out}) R_{GHEX}}{\left(\left(\frac{T_{source, in} + T_{source, out}}{2} \right) - T_{ground} \right)}$$

Where:

G : Mass flow rate of circulation fluid (lb/hr)

C_p : Specific heat of circulation fluid (Btu/lb/F)

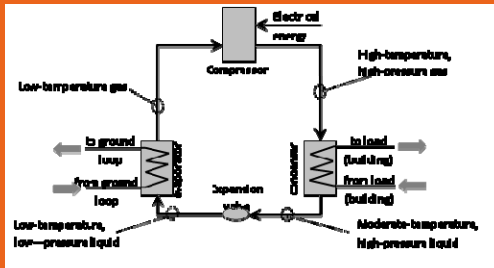
T_{ground} : Undisturbed ground temperature

$T_{source, in}$: Temp. of the fluid entering ground loops

$T_{source, out}$: Temp. of the fluid leaving ground loops

R_{GHEX} : Total thermal resistance of GHEX

G , C_p , and T_{ground} are in fact constant known parameters for a specific design



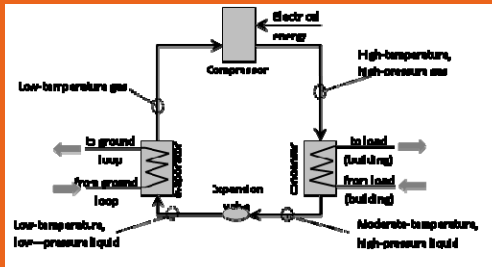
Required GHEX Length (L)

- $T_{source,out}$ controls efficiency of the heat pump. Typically choose;

$T_{source,out} = T_{ground} + (20 \text{ to } 30F)$ for summer

$T_{source,out} = T_{ground} - (10 \text{ to } 20F)$ for winter

- Assuming coefficient of performance (COP) between 2 and 4, then $T_{source,in}$ by;



$$L = \frac{[(8.01 \times 10^3 \times \rho) \times \dot{V} \times (T_{in} - T_{out})] + [W \times 3.413]}{(\rho \times 3.413)}$$

D : density of circulation fluid

\dot{V} : volumetric flow rate of circulation fluid

W : watts of electrical power entering heat pump

Required GHEX Length (L)

Water/antifreeze
mixture properties

UNKNOWN

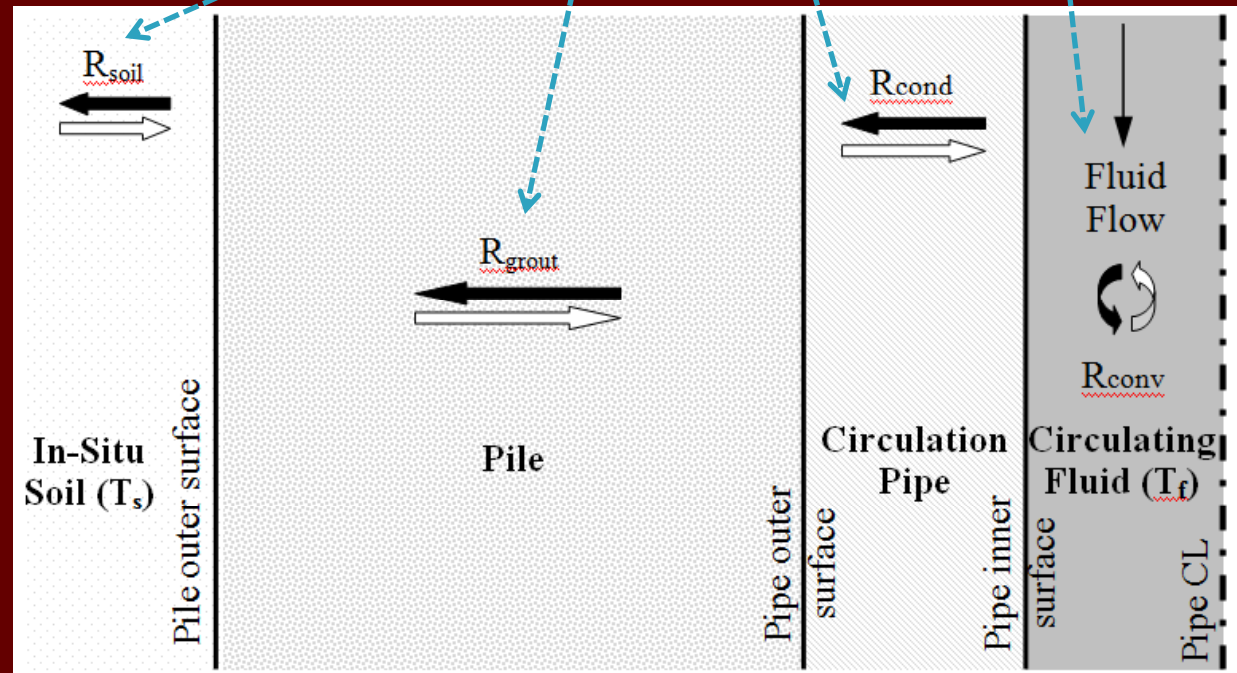
$$\Delta T = \frac{\Delta T_{\text{source, out}} - \Delta T_{\text{site specific}}}{\left(\frac{\Delta T_{\text{source, out}} + \Delta T_{\text{site specific}}}{2} - \Delta T_{\text{from COP}} \right)}$$

from COP related to T_{ground} Site specific (uncontrollable)

Therefore, the less the resistance
the less the required length (L)

Total Resistance of the GHEX

$$R_{total} = R_{soil} + R_{grout} + R_{cond} + R_{conv}$$



Total Resistance of the GHEX

$$R_{\text{GHEX}} = R_{\text{tube}} + R_{\text{grout}} + R_{\text{hole}} + R_{\text{well}}$$

$$R_{\text{GHEX}} = \underbrace{R_{\text{tube}}}_{\text{Site specific (uncontrollable)}} + \underbrace{R_{\text{grout}}}_{\frac{0.5}{\pi d_i h_i}} + \underbrace{R_{\text{hole}}}_{0.5 \frac{\ln(d_o/d_i)}{2\pi\lambda_p}} + \underbrace{R_{\text{well}}}_{\frac{1}{2\pi\lambda_g} \ln\left(\frac{d_b}{\sqrt{2}d_o}\right)}$$

where;

d_i : inner diameter of the tube

d_o : outer diameter of the tube

d_b : borehole diameter

λ_p , and λ_g : thermal conductivities of tube and grout, respectively

Total Resistance of the GHEX

$$R_{\text{grout}} = \frac{1}{2\pi\lambda_g} \ln\left(\frac{d_b}{\sqrt{2}d_o}\right) \quad R_{\text{pile}} = \frac{0.5}{\pi d_i h_i} \quad R_{\text{tip}} = 0.5 \frac{\ln(d_o/d_i)}{2\pi\lambda_p}$$

- Since changes in d_o , d_i , and λ_p is not significant for typical applications. Then, only R_{grout} can be reduced.
- *Using thermal grout increases λ_g .*
- Smaller d_b gives lower R_{grout} .
- Then, micropiles are better than large diameter piles or caissons