

# CYCLIC QUASI-STATIC LOAD TESTS ON MICROPILES

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- Wet & Dry Shotcrete
- Structural Shotcrete
- Seismic Anchors
- Micropiles / Minipiles
- Cementitious Grouting
- Chemical Grouting

- **Recently, 212 GEWI-Piles were installed in New Westminster, BC, to support a 20,000 m<sup>3</sup> partially submerged buried storage tank subject to cyclic loading.**
- **Following, two pre-production full scale verification cyclic load tests are reviewed**
- **“Cyclic” loading, as described in this paper, refers to quasi-static alternating compression and tensile loads, with no dynamic component. Details of this type of pile response are provided.**
- **The GEWI-Piles were installed by a local specialty foundation contractor, Southwest Contracting Ltd.**





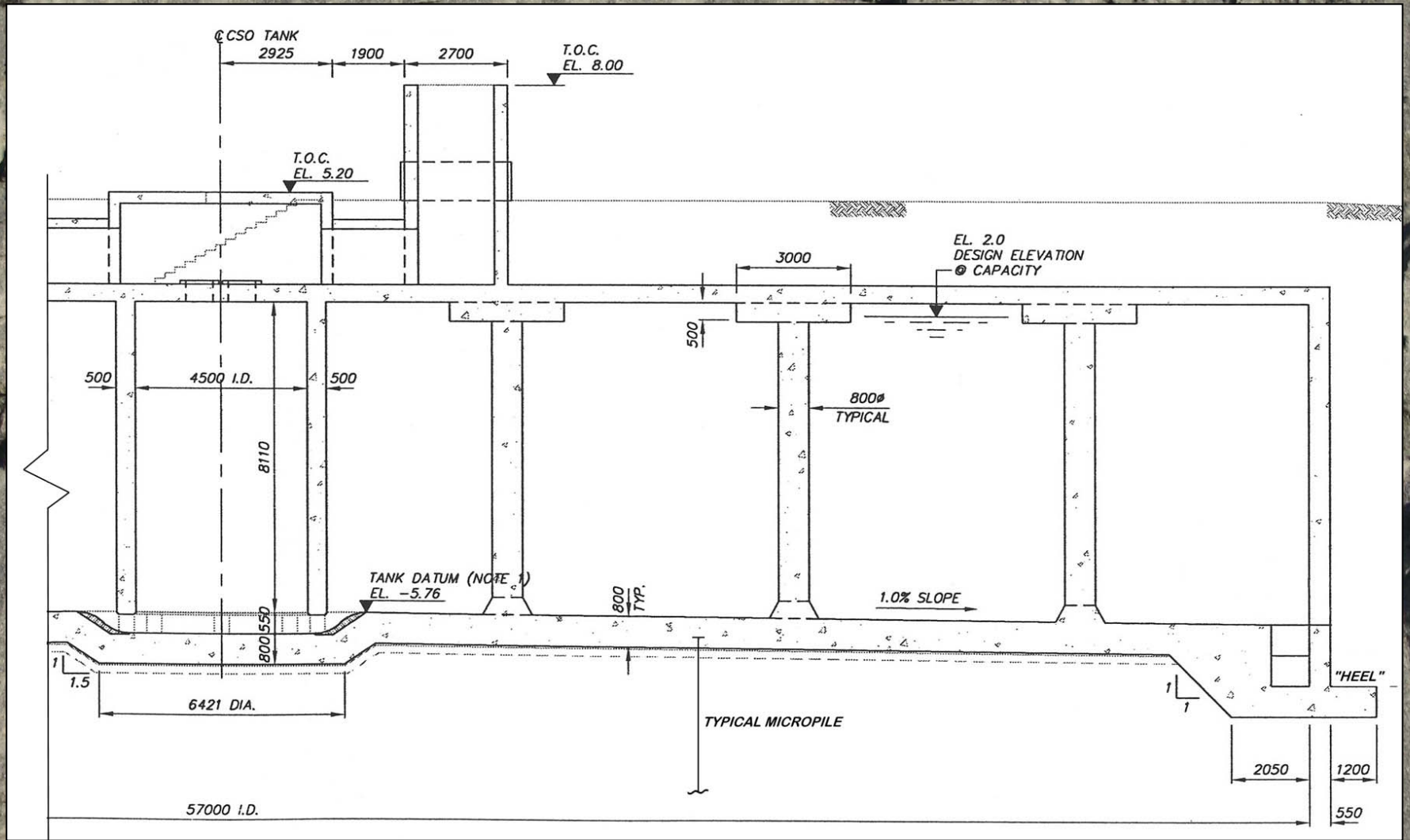


Figure 2b. Tank Section

# DESIGN

- The tank structure required foundations to resist uplift forces due to buoyancy caused by groundwater table rise and compression forces caused by filling of the tank.

## *Cyclic loading per GEWI-Pile:*

- Max. factored tension load = 380 kN
- Max. working tension load = 200 kN
- Max. working compression load (including 12 mm creep effect) = 600 kN
- Max. working compression load (no creep effect) = 140 kN

## *“Heel”*

- The Engineers designed the “heel” to resist uplift forces due to buoyancy along the perimeter of the tank so no cyclic effects.
- Long term creep in the soils near the centre of the tank was anticipated to be, as much as, 12 mm.

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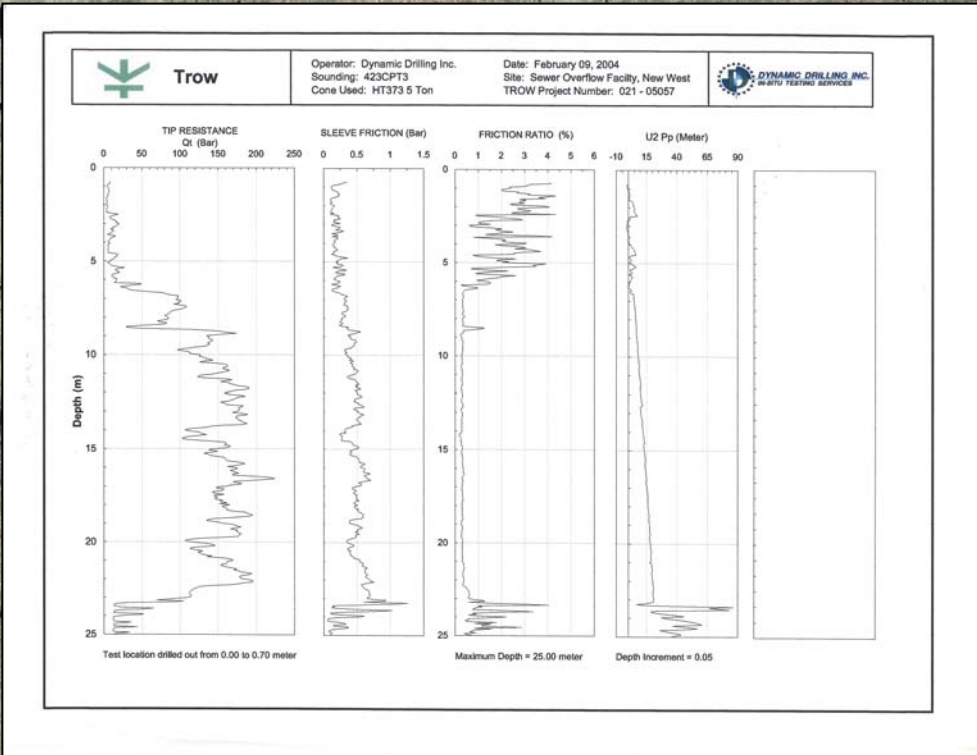


Table 1. Generalized Soil Profile

Soil Unit	Thickness	Description
Unit a1	0 to 1.5 m	silty sand, sandy silt – FILL
Unit a2	4 to 5 m	soft to firm sandy SILT - FILL?
Unit b1	2 to 2.5 m	loose to medium dense sand
Unit b2	12 to 15 m	medium dense to dense SAND
Unit c	> 2 m	interbedded SILT or CLAY and SAND

Figure 1. CPT04-3 Log

(Uthayakumar and Macleod 2004)



**Drill string advancement**

**Due to the sandy soils and high groundwater table, a cased direct circulation drill system was specified with the objective to minimize disturbance at the soil-grout interface and ground loss.**

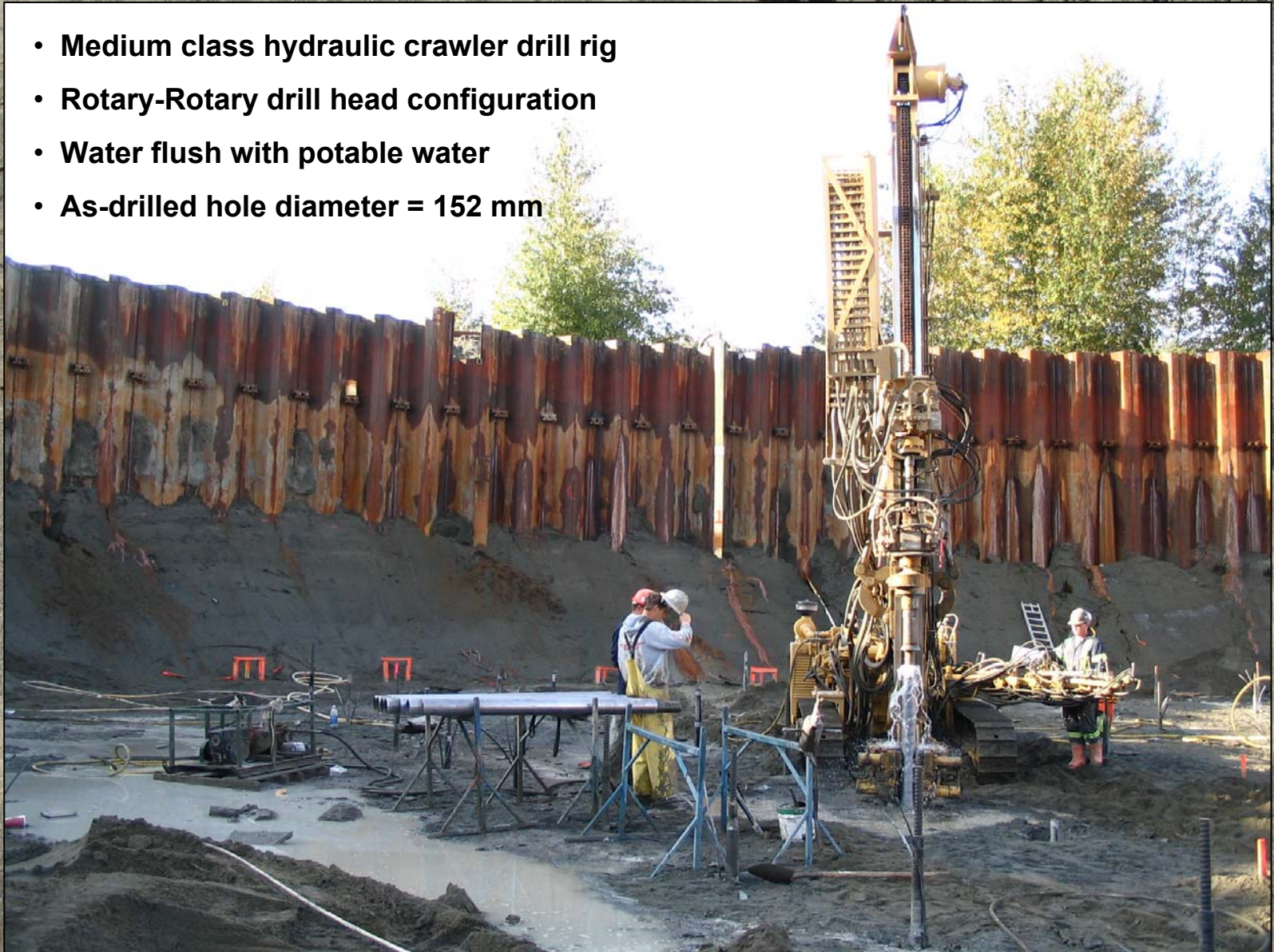
- **Disposed cuttings shall not exceed 110% of the theoretical drill hole volume.**
- **Casing shall not have an O.D. < 133 mm**
- **The use of air drilling is not permitted**
- **Drilling using augers is not permitted**



- Drilling was performed inside a full cut-off wall, extending to a silt/clay layer at -22 m elevation located at the crest of a sloped excavation.
- The drill hole was advanced from -6.8 m elevation during on-going dewatering activities.
- Diesel/hydraulic rig utilizing double head duplex overburden drilling method advanced a 133 Ø temporary casing.



- **Medium class hydraulic crawler drill rig**
- **Rotary-Rotary drill head configuration**
- **Water flush with potable water**
- **As-drilled hole diameter = 152 mm**





- Full length GEWI-Piles were installed using a zoom boom type machine
- No couplers used since GEWI-Piles ordered full-length from the factory.
- GEWI-Piles installed immediately after drilling then tremie grouted

- **Microsil Anchor Grout**

A high early strength, thixotropic, cement grout

- **Water : Cement Ratio < 0.35 was specified**

- **Primary grouting to 517 kPa minimum**

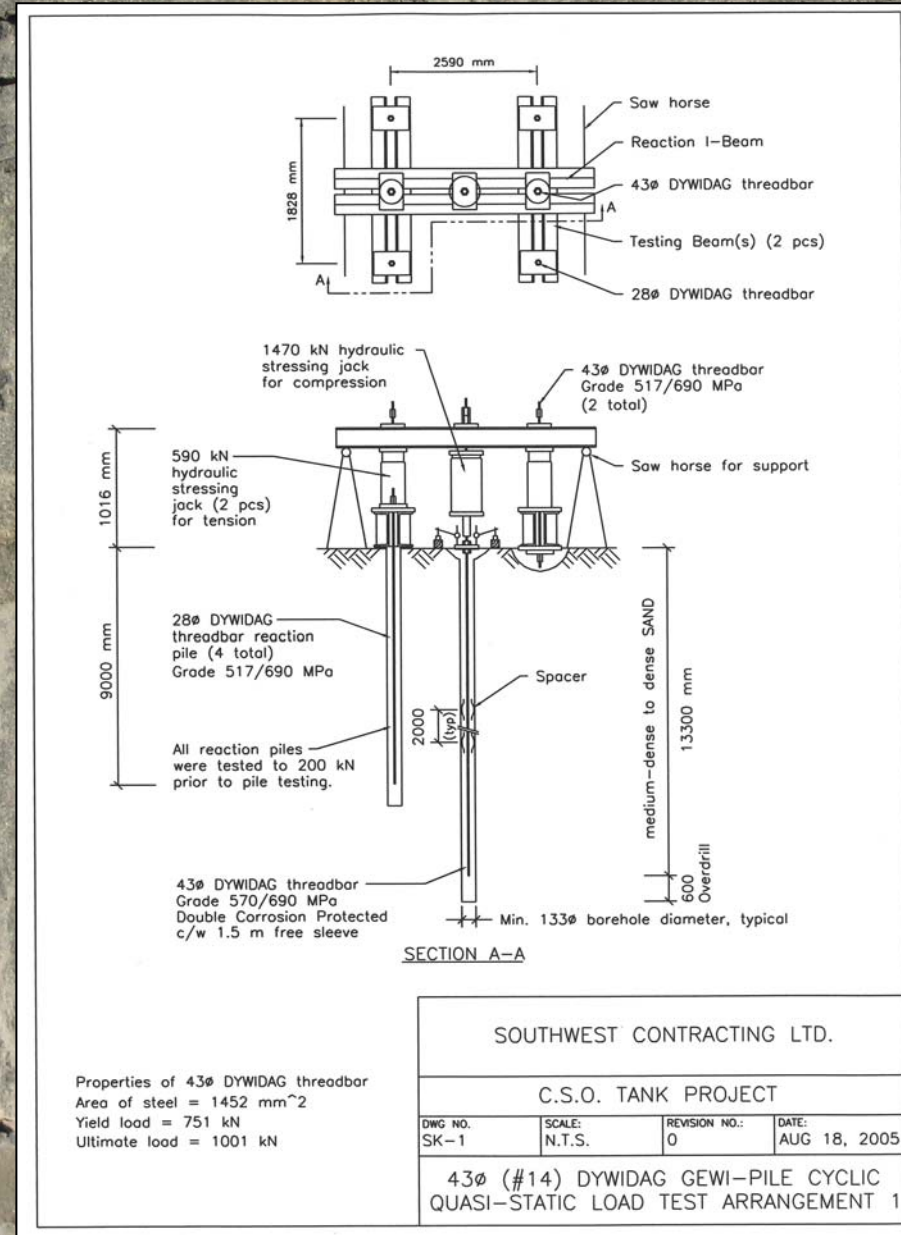
- **Pressure grouting thru the top of the casing at intervals as the casing was being pulled.**

- **One stage of post-grouting to 5,170 kPa minimum was performed prior to any testing.**

- **A subsequent test program, on-site, showed post-grouting had little influence on test results.**



- Reaction I-Beam repeatedly tilted during tension loading and translated laterally due to slight off-centered loading.
- Further alterations to the initial framework were ruled out. Consequently the jacking arrangement was modified.
- During each load reversal the top nuts of each reaction pile and test pile were loosened and tightened, respectively, in order to change loading direction.

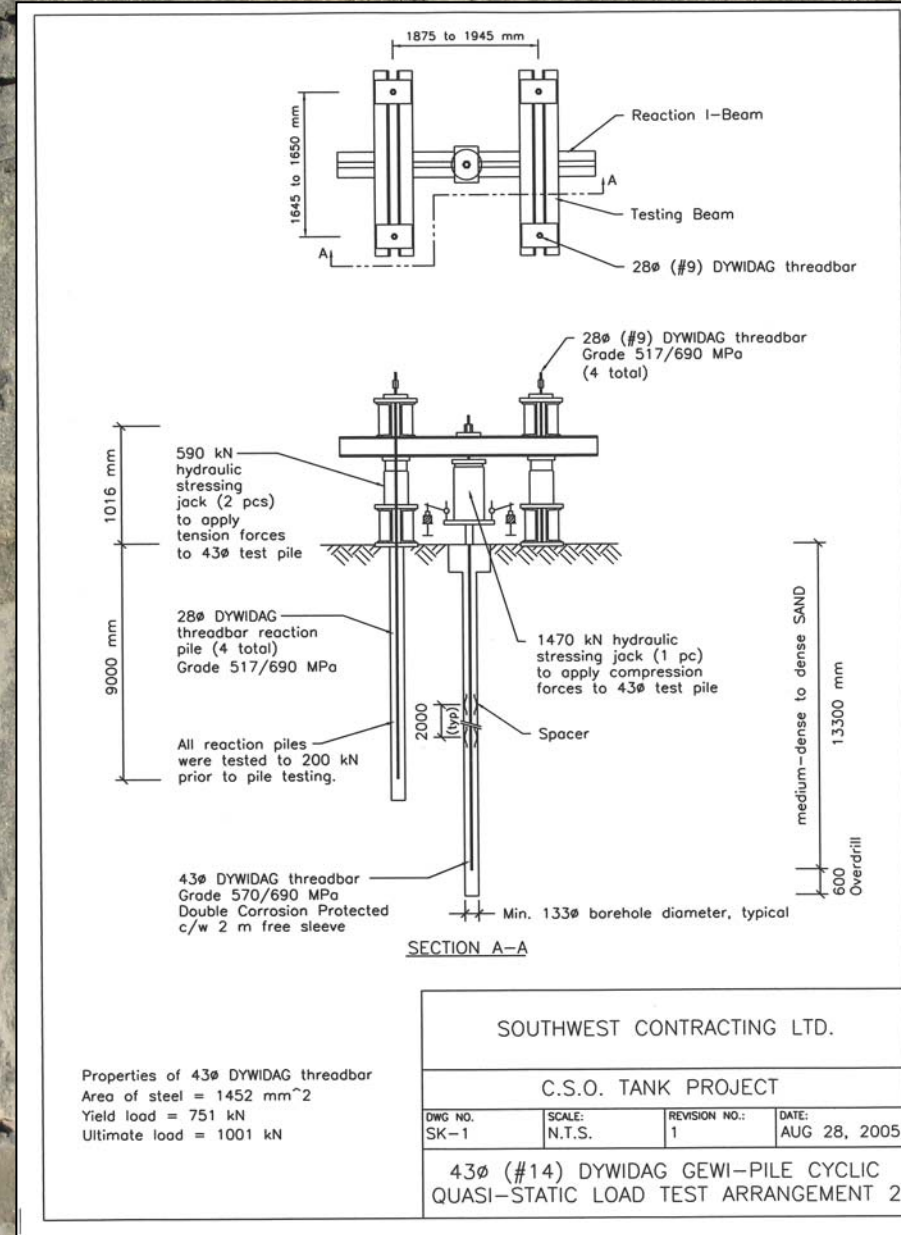


**Test setup 1**

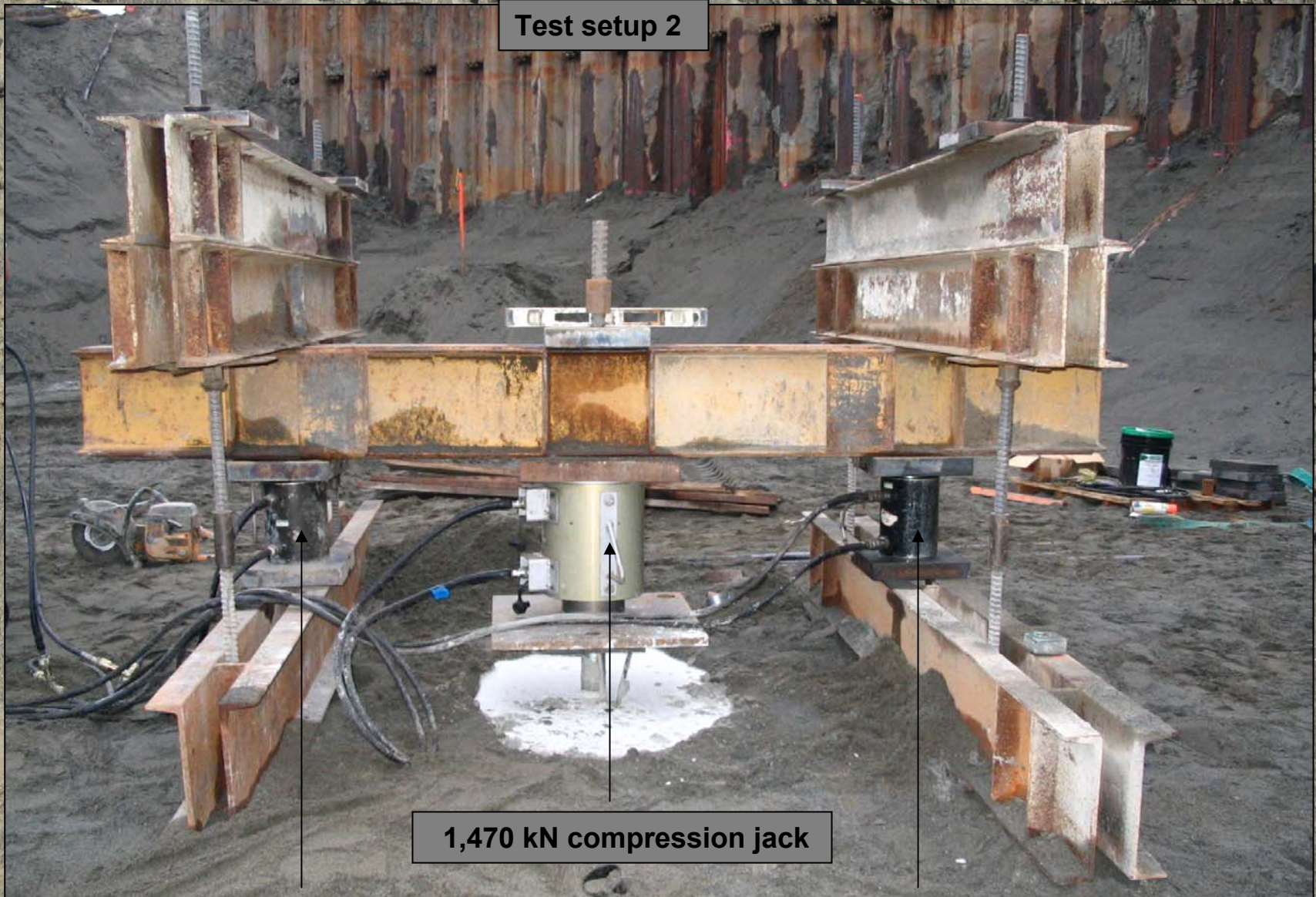


Test setup 1

- Added test beams overtop the original test setup
- Test setup did not meet ASTM standards with respect to spacing of the reaction piles and test pile. No standard was specified during tendering.
- Recommend future test setups meet ASTM standard D3689 for tension tests and ASTM D1143-81 for compression tests.



**Test setup 2**



Test setup 2

1,470 kN compression jack

Two 590 kN tension jacks synchronized by hydraulically connecting each to the same hydraulic power pack.

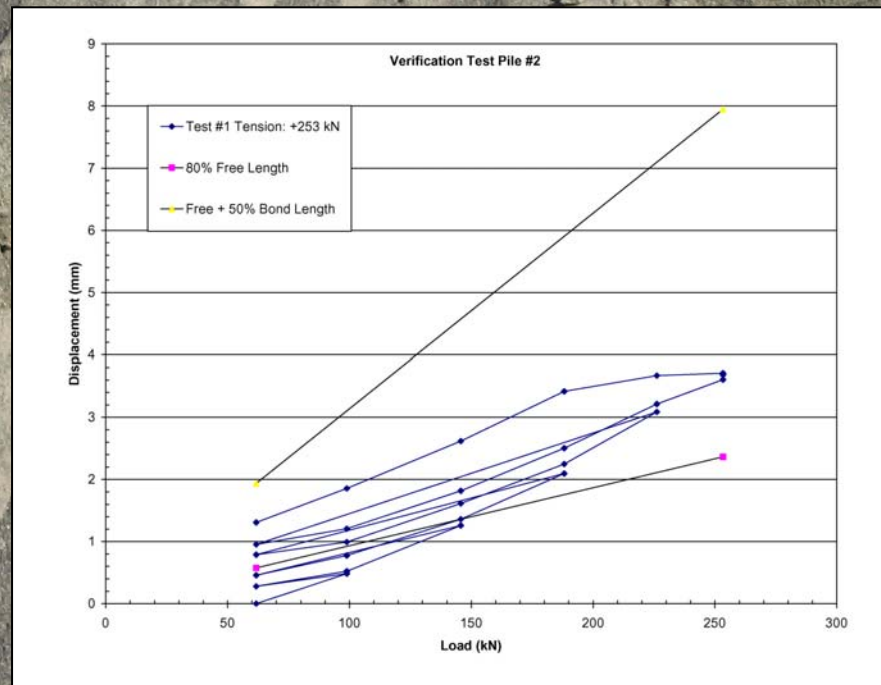
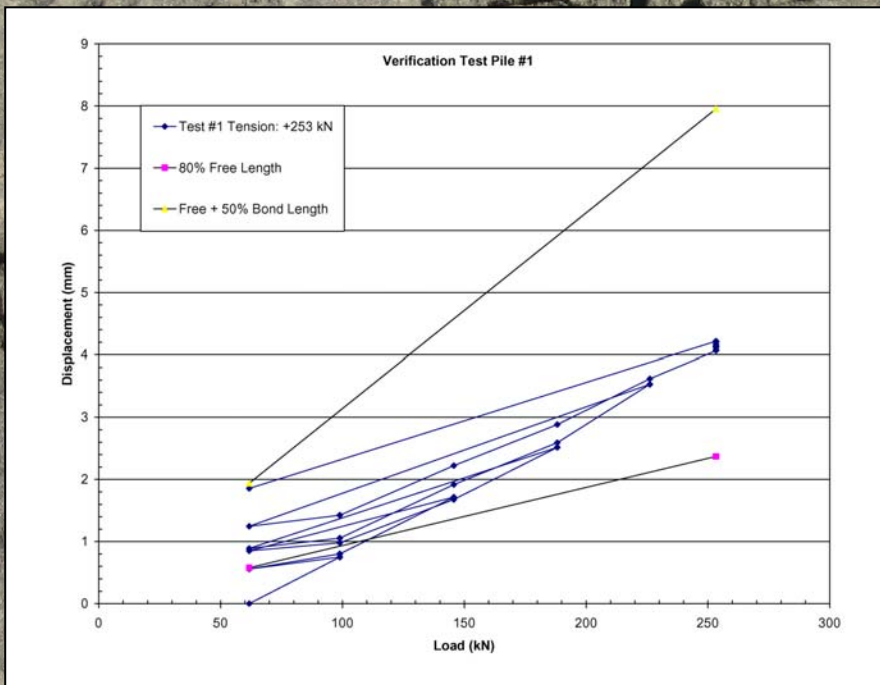


Four performance verification tests in total were performed on each test GEWI-Pile in the following sequence:

1. A 250 kN tension test in accordance with PTI-1996.
2. A 175 kN compression test in accordance with PTI-1996
3. A cyclic test starting from a 250 kN tension alignment load to 600 kN compression load by increasing compression loading 75 kN each successive cycle.
4. A 450 kN tension test in accordance with PTI-1996

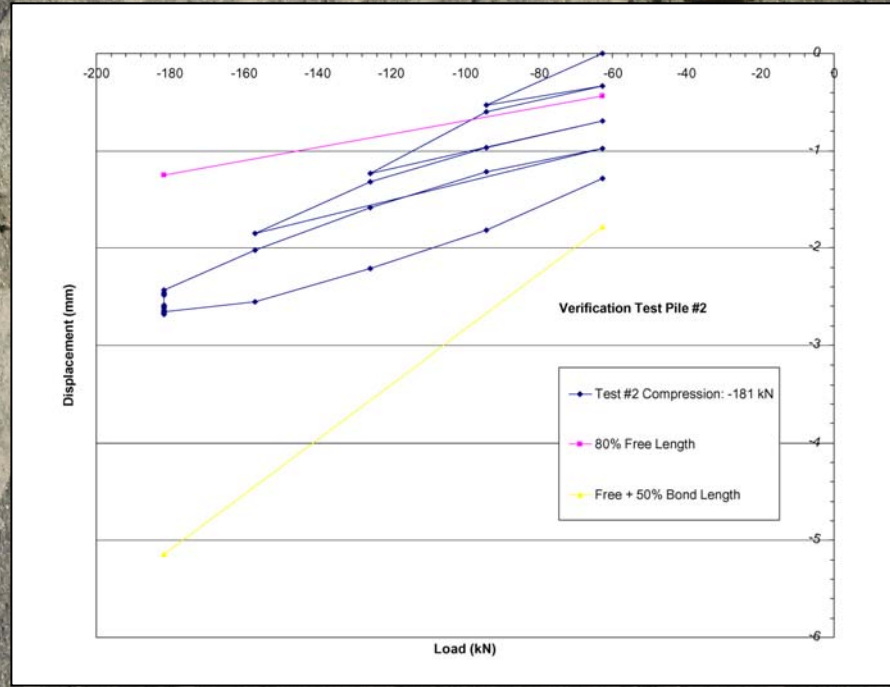
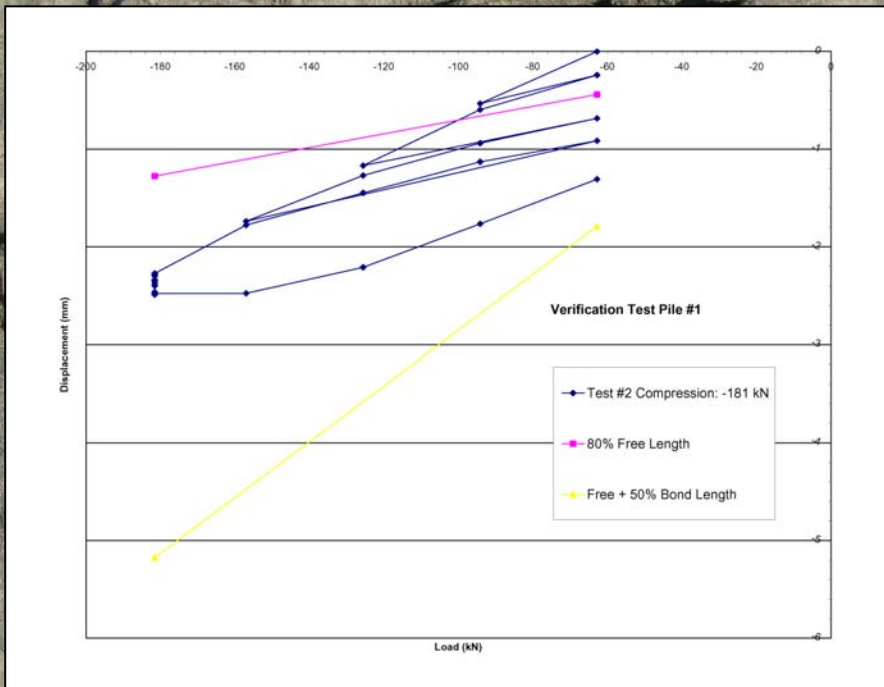


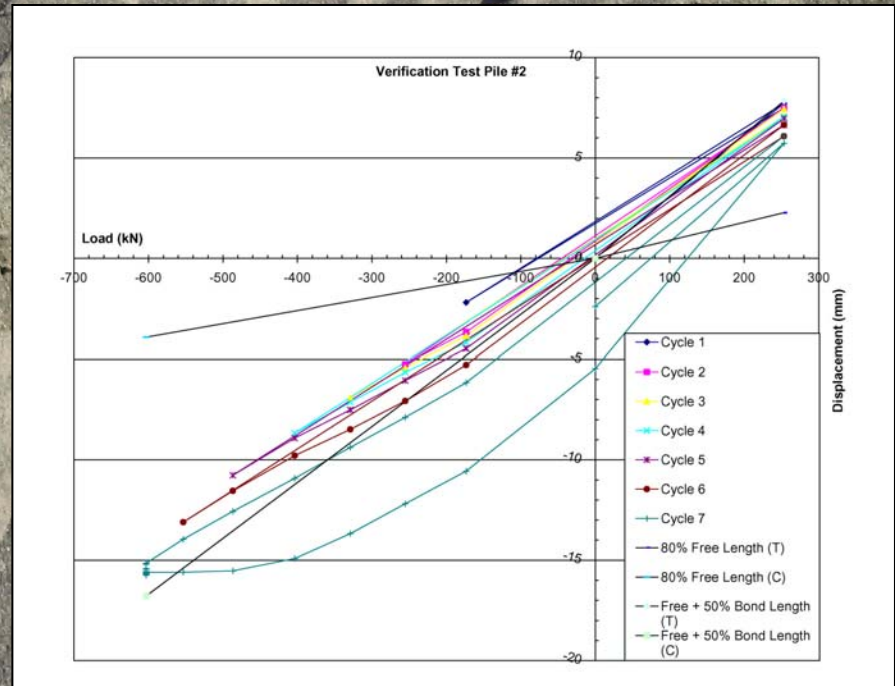
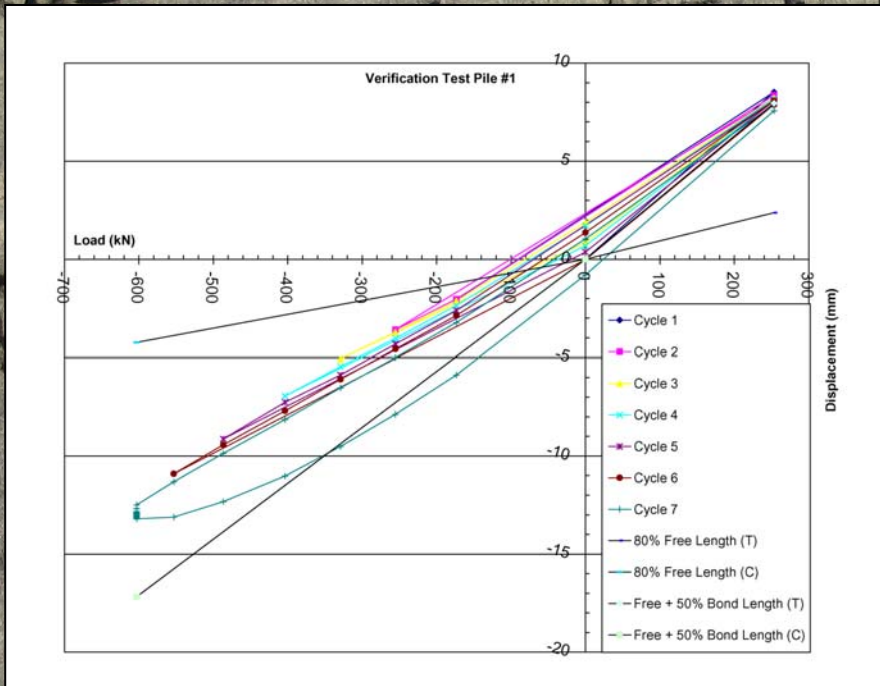
Grout Collar isolated from the pile



# PERFORMANCE & EXTENDED CREEP TEST RESULTS

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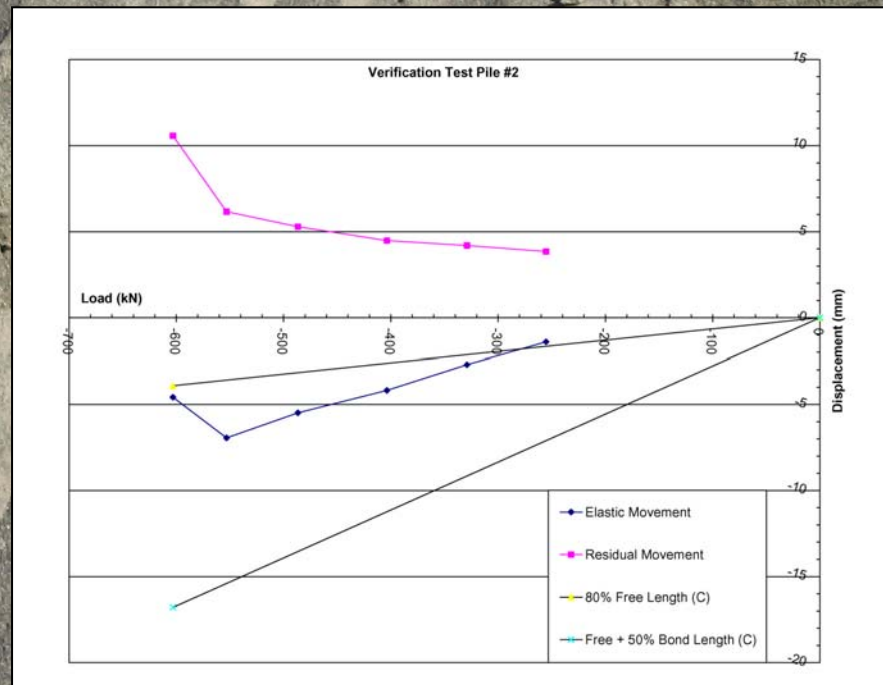
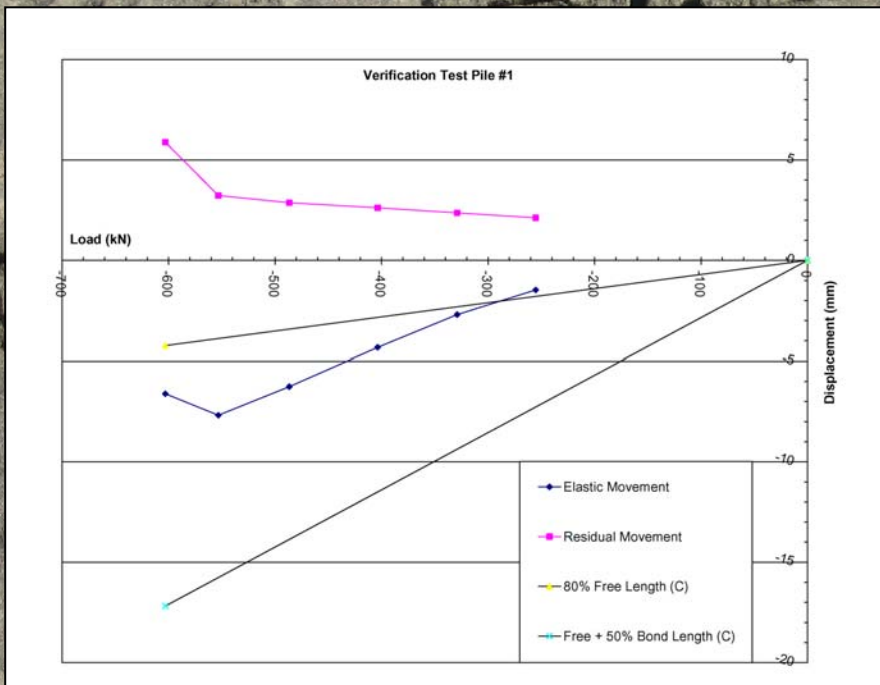


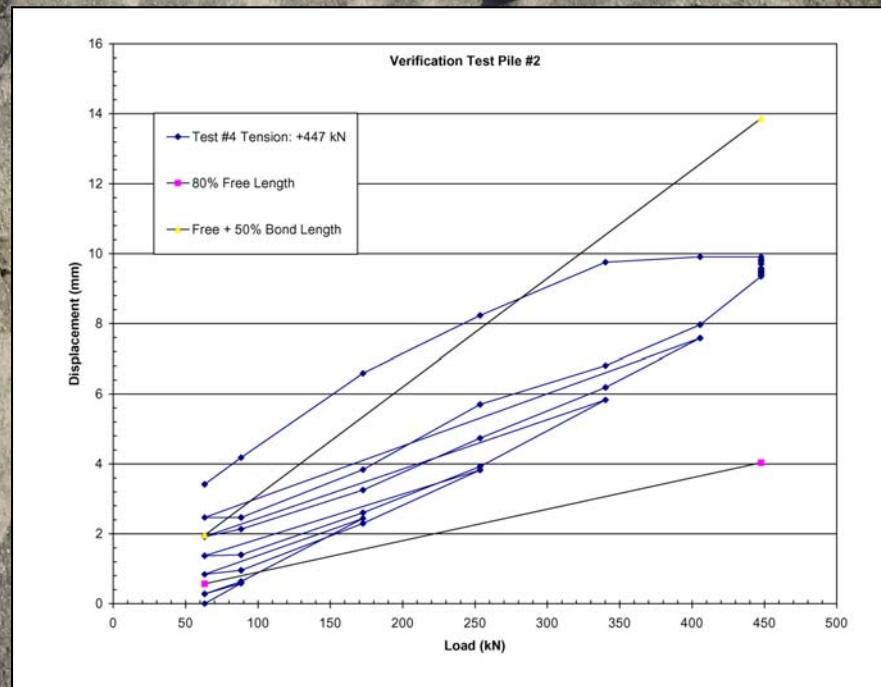
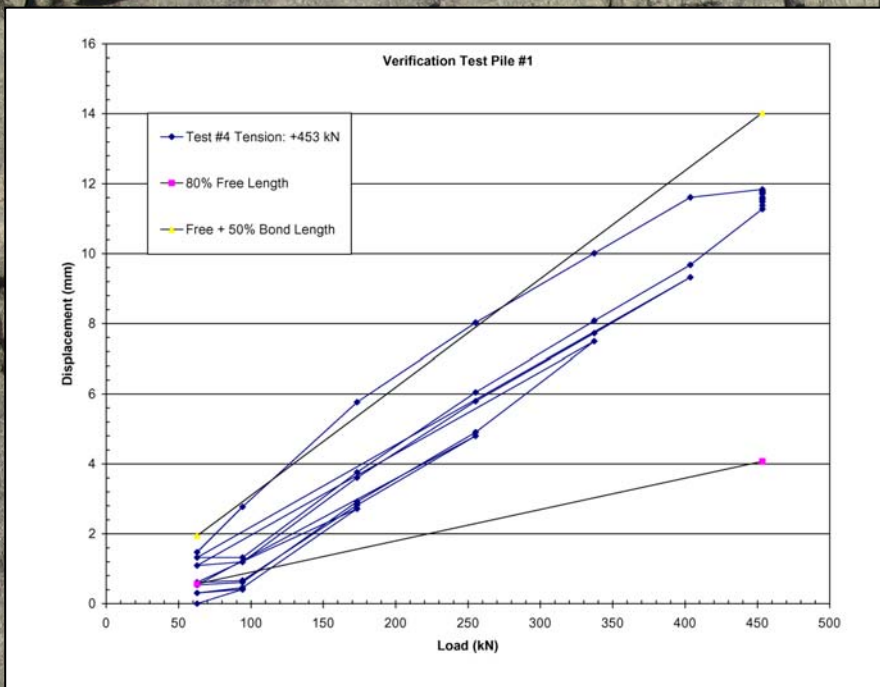


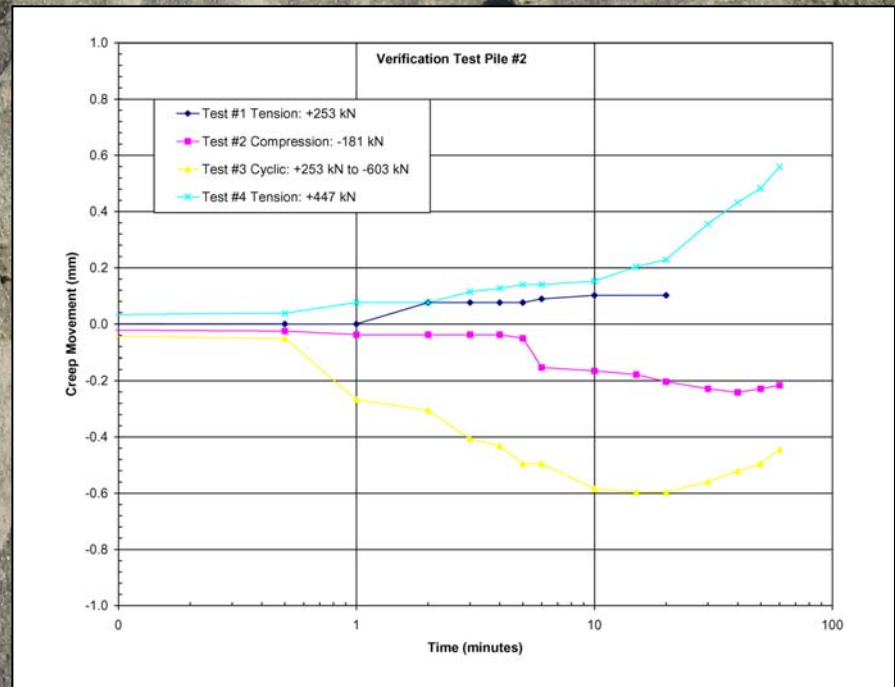
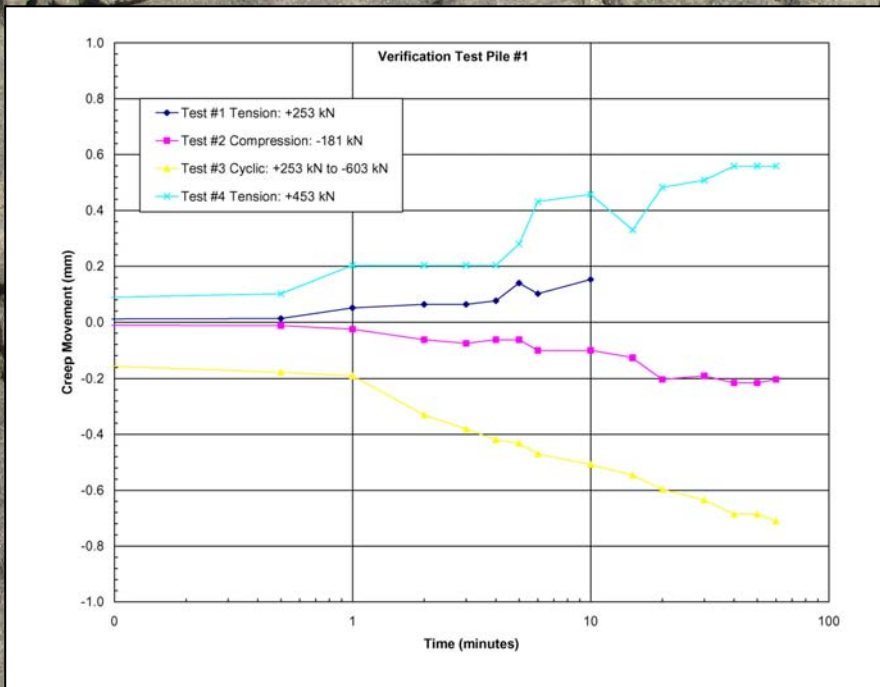
**The shape of cycle 7 shows similar unloading stress histories and shows departure from a linear, reproducible cyclic loading pattern.**

# PERFORMANCE & EXTENDED CREEP TEST RESULTS

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**Log-linear increasing displacement to – 0.71 mm during the final two log cycle**

**Non-log-linear displacement to – 0.61 mm during the final two log cycle**

**Based on the test results of the two verification cyclic load tests, the installed GEWI-Piles were considered adequate to sustain their design loads**



## Recommendations

- 1. Use of strain gauges in future tests to determine shape of the load distribution along the fixed anchor and its behavior under cyclic loading**
- 2. Repeated cyclic loading at design load to determine how the number of load cycles affects load holding capacity.**