

DEVELOPMENT OF A DESIGN, INSTALLATION AND TESTING FEEDBACK MODEL FOR MICROPILES IN PROJECTS WITHOUT EXTENSIVE GEOTECHNICAL INFORMATION

Allan Herse B.Eng (Civil), MIEAust, CPEng, RPEQ

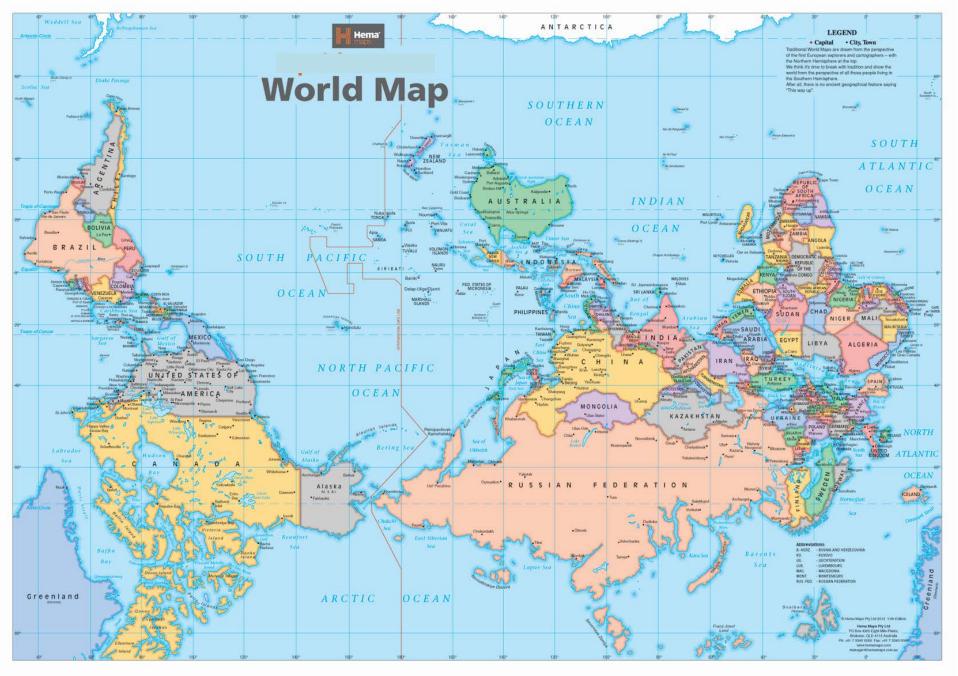




DEVELOPMENT OF A DESIGN, INSTALLATION AND TESTING FEEDBACK MODEL FOR MICROPILES IN PROJECTS-WITHOUT EXTENSIVE GEOTECHNICAL INFORMATION

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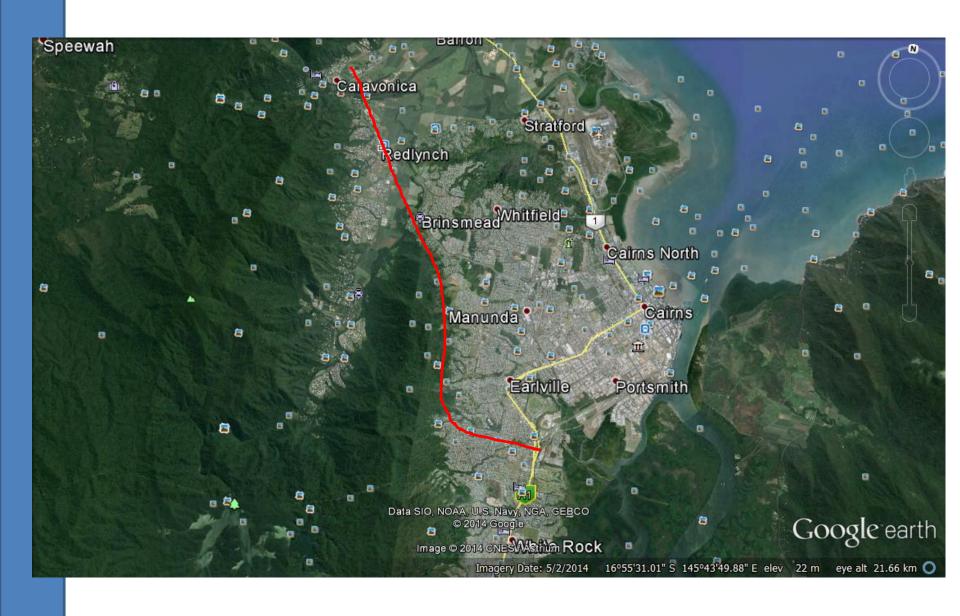










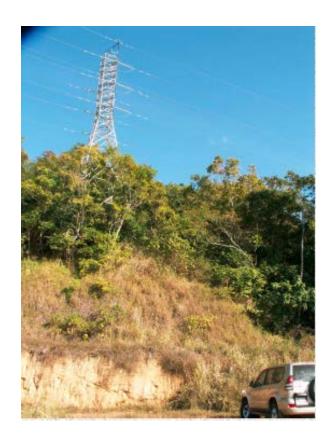




Foundations at the end of their design life







Challenging Locations

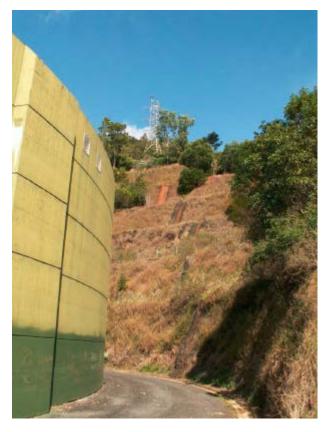






Needed to keep new foundations as small as possible to minimise visual impact and construction materials











Hollow bar micropile solution was proposed

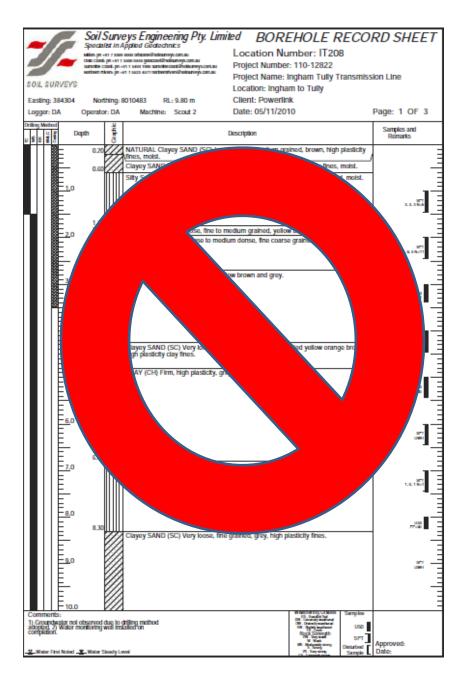








No soils information....what to do?



- Live power lines made it difficult for geotechnical drilling beneath towers
- Access restrictions within residential areas
- Steep terrain
- Time
- Cost



Traditional design and installation sequence













Then we remembered what Nadir always says about having a customer with a need







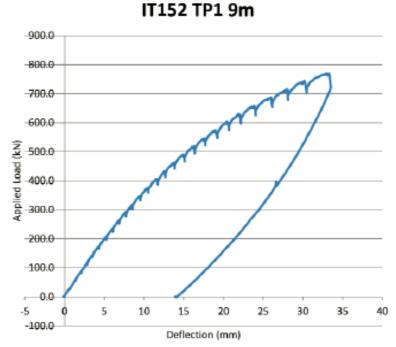


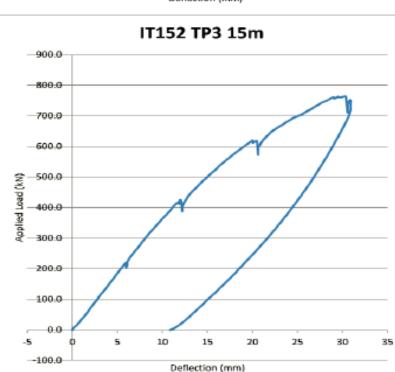
Site IT152 — What do we think?

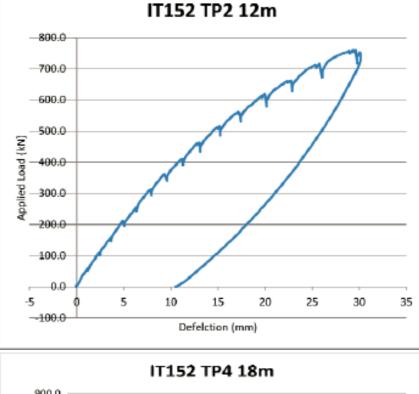
Layer Number	Soil Description	Layer position	SPT "n" value
1	Clayey Silt, Firm to Stiff	0-1.2m	N/A
2	Clayey Sand and Gravel, Medium Dense	1.2m-2.5m	13
3	Sand and Gravel, Loose	2.5m-4m	4
4	Silty Clay, Hard	4m-5.8m	40
5	Sandy Silty Clay, Hard	5.8m-7.2m	36
6	Sandy Silt, Stiff	7.2m-9.7m	10
7	Silty Sand, Loose	9.7m-11.8m	5 & 11
8	Sand, Medium Dense	To limit of tests	14 to 20

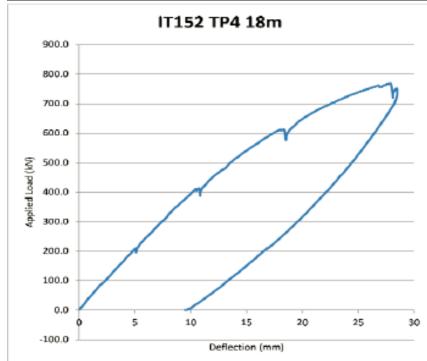
Design load estimate of the 9m pile was 250kN (56kips) if using AS2159 and values of skin friction based on Ischebeck data

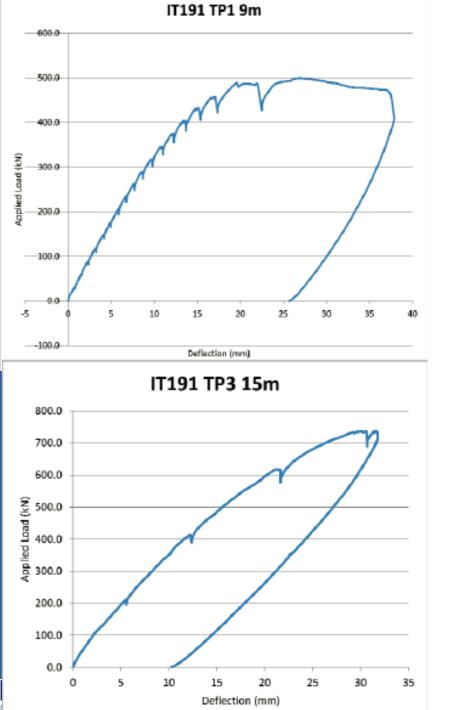


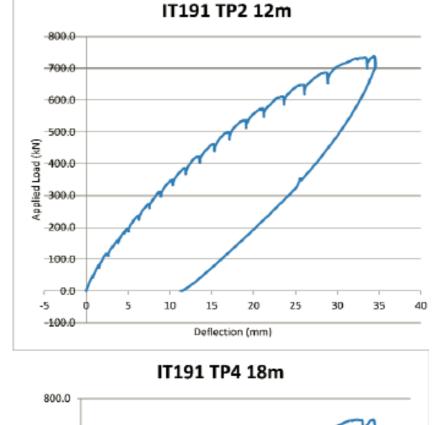


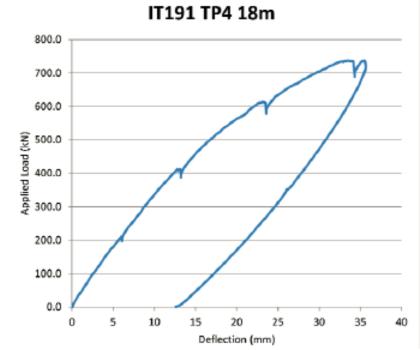


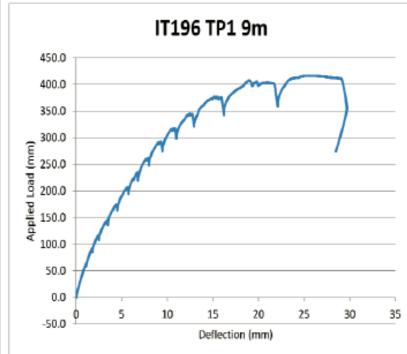


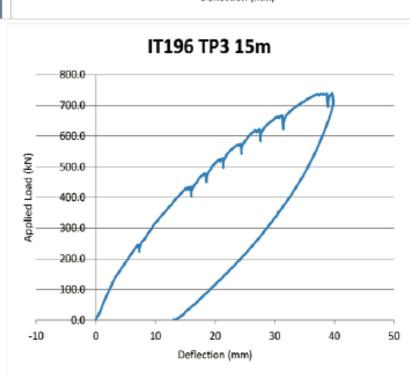


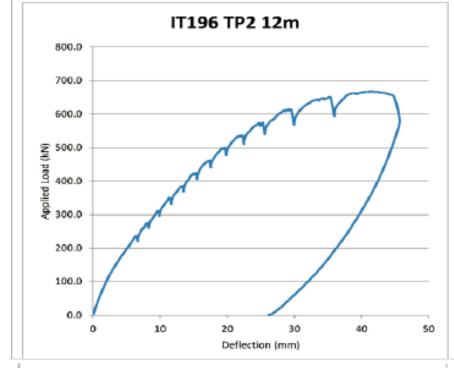


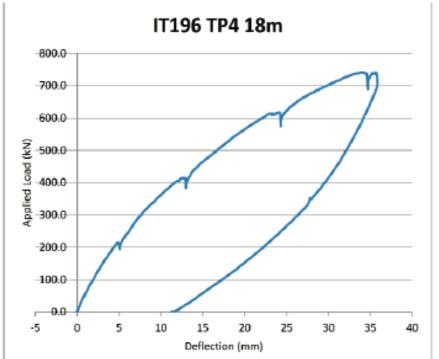


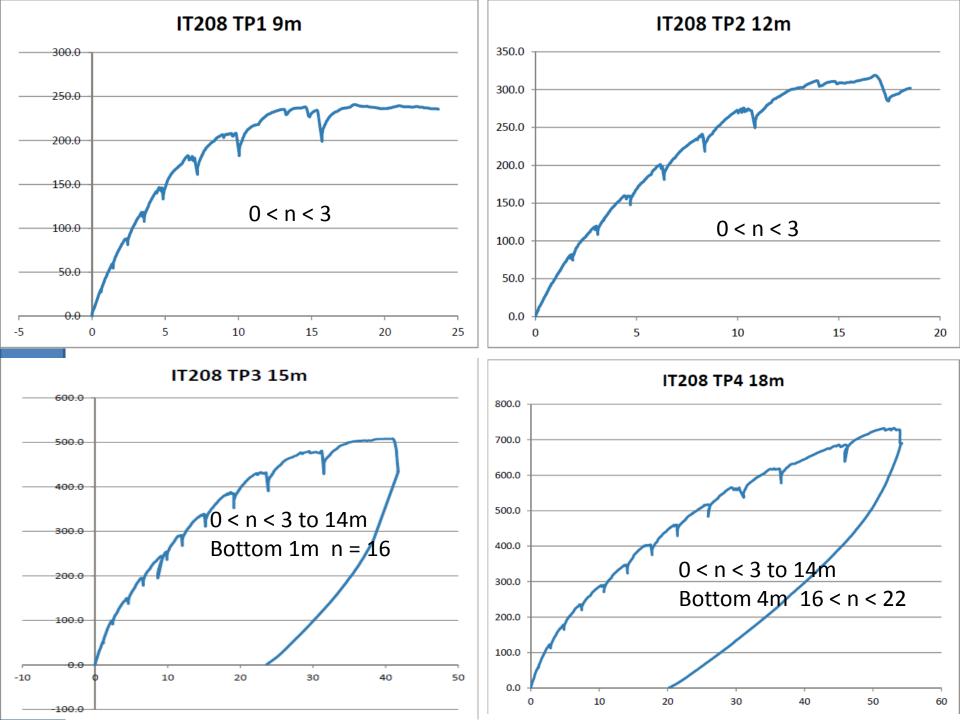












ULTIMATE SKIN FRICTION

The ultimate geotechnical capacity of the soils can be determined from the following formula;

$$q_{usk} = \frac{R_{us}}{L\pi D}$$

Where:

R_{us} = Ultimate Structural Capacity of the pile

L = Pile Length

 $\pi = Pi$

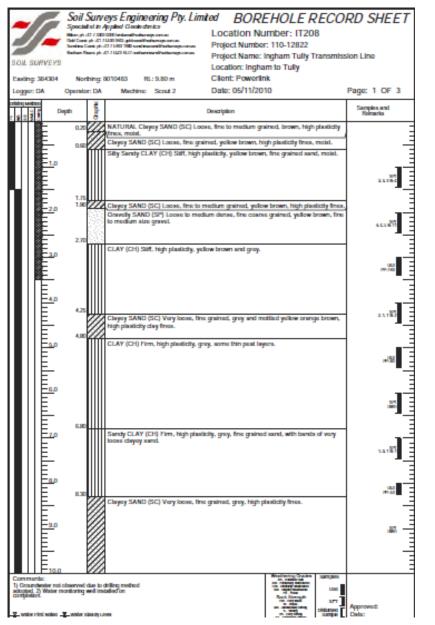
D = Diameter of the pile in contact with the soil

qusk = Ultimate Skin Friction (kPa)

Pile	Ultimate Skin Friction			
Length	IT152	IT 191	IT196	IT208
m	kPa	kPa	kPa	kPa
9	112	89	56	40
12		99	78	41
15			77	50
18				54
	Coloured cell indicates piles tested to steel yield			
	and provide approximate UGC			



Comparison with soils information



Site IT208

Layer Number	Soil Description	Layer position	
1	Clayey Sand, Loose	0-0.6m	
2	Silty Sandy Clay	0.6m-1.75m	
3	Clayey Sand, Loose	1.75m-1.9m	
4	Gravelly Sand, Loose to Medium Dense	1.9m-2.7m	
5	Clay, Stiff	2.7m-4.25m	
6	Clayey Sand, Very Loose	4.25m-4.8m	
7	Clay, Firm	4.8m-6.8m	
8	Sandy Clay, Firm	6.8m-8.3m	
9	Clayey Sand, Very Loose	8.3m-13.7m	
10	Sandy Clay, Very Stiff	13.7m-13.9m	
11	Clayey Sand, Medium Dense	13.9m-15.9m	
12	Sand, Medium Dense	15.9m-17 m	
13	Gravelly Sand, Medium Dense	17m-19.8m	
14	Sandy Clay, Hard	19.8m-20.2m	
15	Sand, Medium Dense	20.2m-20.5m	

Pîle	Ultimate Skin Friction			
Length	IT152	IT 191	IT196	IT208
m	kPa	kPa	kPa	kPa
9	112	89	56	40
12		99	78	41
15			77	50
18				54
	Coloured cell indicates piles tested to steel yield			

and provide approximate UGC



Analysis was also done on:

- 1. Rate of advance for each lin.m of pile installed
- 2. Degree of use for the top hammer of the drill per lin.m

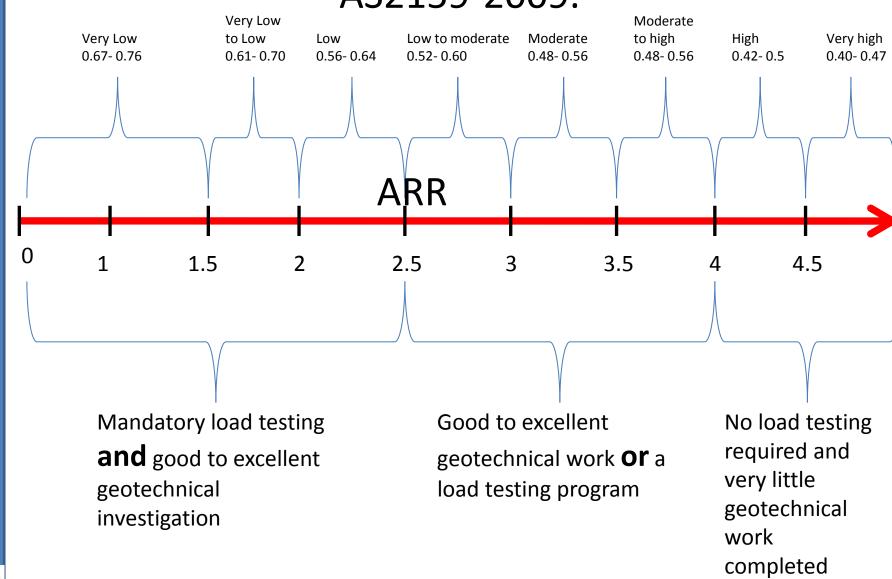


From this information, we developed an approximation for capacity per lin.m related to the observed drilling conditions.

- 1. Rotary only no top hammer = W kN/lin.m
- 2. Top hammer < 2min/m = X kN/lin.m
- 3. Top hammer between 2 & 5min/lin.m = Y kN/lin.m
- 4. Top hammer greater than 5min/lin.m = Z kN/lin.m

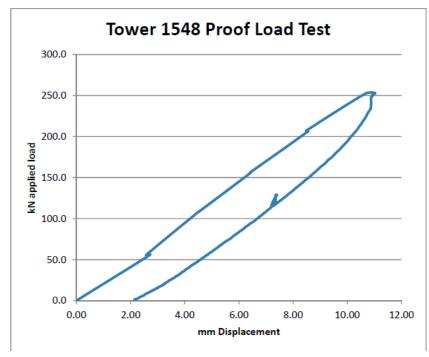


This value was factored down by a geotechnical reduction factor (ϕ_g) from Australian Standard AS2159-2009.

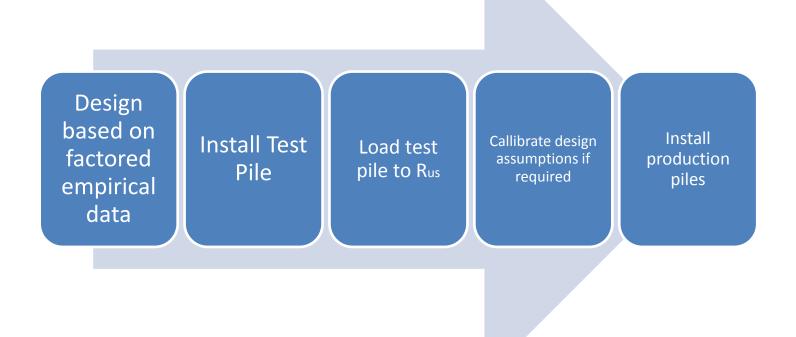




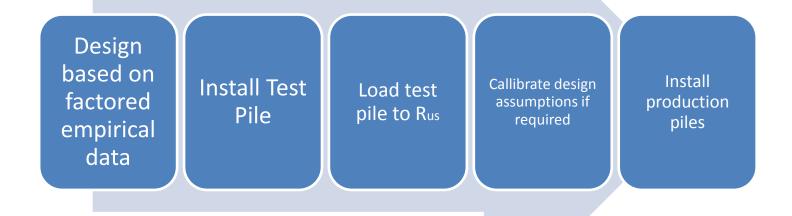
Verification testing was carried out on each site



Design, installation and testing feedback model was created for production pile installation



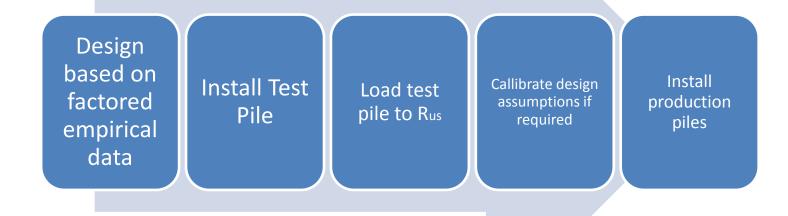




Some critical factors for success in using this model;

- 1. Design values need to be calibrated to the drill rig
- 2. Driller needs to have a clear set of instructions to understand the design intent. More than ever, they are in control of the end result
- 3. Supervision needs to be at a high level.
- 4. Client needs to understand the cost is not known until piles are installed

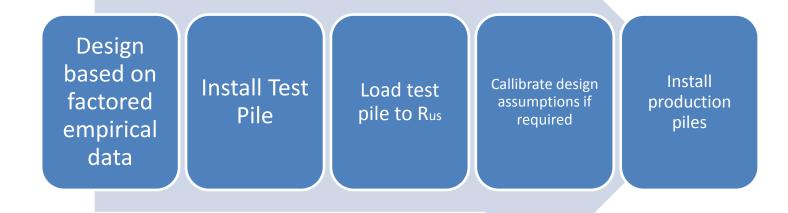




Main advantages

- 1. Enables projects to be undertaken where it may be impossible or cost prohibitive to obtain good geotechnical data
- 2. Speeds up delivery of a project by not having to wait for geotechnical data
- 3. The cost of the sacrificial test pile is equivalent to the cost of good geotechnical information but produces an arguably more reliable result





Main disadvantages

- 1. Difficult for owner to know the cost of a project and develop a reliable budget. They need to be committed to the project
- 2. Requires highly skilled crews and supervision
- 3. Can limit the number of bidders on a project due to the need to calibrate the design values against the drilling equipment



Thank you



