



REVIEW OF FRENCH “FOREVER” PROJECT
Prof. Schlosser, Terrasol and Dr. Frank, ENPC-CERMES, France



FOREVER

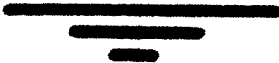
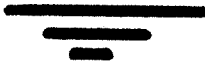
Projet National : Renforcement des sols par micropieux

"FOREVER"

FRENCH NATIONAL RESEARCH PROJECT

Prof. François SCHLOSSER. TERRASOL Consulting Co.

Prof. Roger FRANK. CERMES (ENPC - LCPC)

- 
- ① MAIN ASPECTS
 - ② PRESENT DESIGN
 - ③ RESEARCH PROGRAM
 - ④ SLIDES , if time allows...
- 

MAIN ASPECTS OF THE RESEARCH

① SINGLE MICROPILES

Settlement estimation

Horizontal forces (calibration chamber, centrifuge,
full scale measurements)

Buckling

Durability

Seismic behaviour

② GROUPS OF MICROPILES

Mechanical interaction (vertical forces)

Horizontal forces

Effect of the pile cap

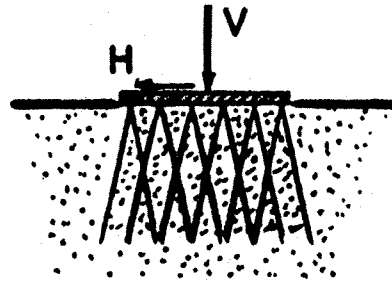
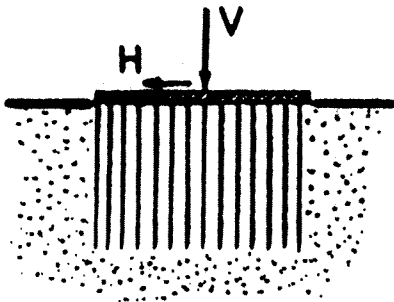
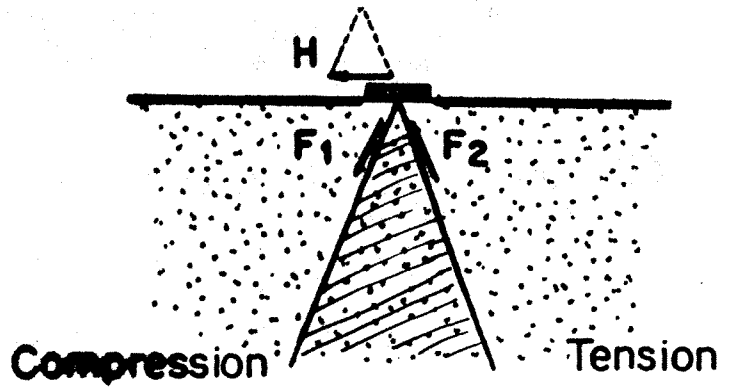
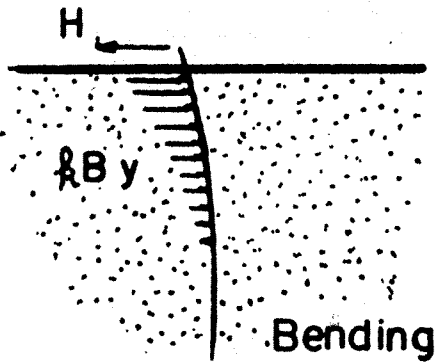
③ NETWORKS OF MICROPILES

Experimental behaviour (calibration chamber,
shear box, full scale instrumentations) under
forces.

Modelization and theoretical studies

Design method for groups and networks

MICROPILES : STRUCTURAL EFFECT



MAIN GOALS OF THE "FOREVER" PROJECT

BEHAVIOUR AND DESIGN

- Deep foundation
- Underpinning
- Slope stabilization
- Settlement reduction

RESEARCH TOOLS

Monitoring on construction sites

Tests on experimental sites

**FULL
SCALE**

Laboratory models (1g)

Centrifuge models

Numerical modelling

**BASIC
BEHAVIOUR
+
PARAMETRIC
STUDY**



FOREVER

Projet National : Renforcement des sols par micropieux

PRESENT DESIGN OF MICROPILES

- ① Bearing capacity**
- ② Overall stability (slope stabilization)**
Numerical analysis

TRADITIONAL DESIGN

COMPRESSION : $Q_u = Q_u^p + Q_u^s$
tip Frictional

TRACTION : $Q_{tu} = Q_u^s$

TIP RESISTANCE

$(Q_u^p = 0 \text{ to } 0.15 Q_u^s)$

$Q_u^p = S_p \cdot k_p \cdot p_\ell$

- $k_p = \begin{cases} 1.2 & \text{Gravels and Sands} \\ 1.6 & \text{Clays} \\ 1.8 & \text{Clays and Marls} \\ 1.5 & \text{Altered Rocks} \end{cases}$

$S_p = \frac{\pi}{4} \cdot D_d^2$

$p_\ell =$ limit pressure at pressuremeter test

FS = 3

FRICTIONAL RESISTANCE

$Q_u^s = \pi \cdot D \cdot L \cdot q_s$

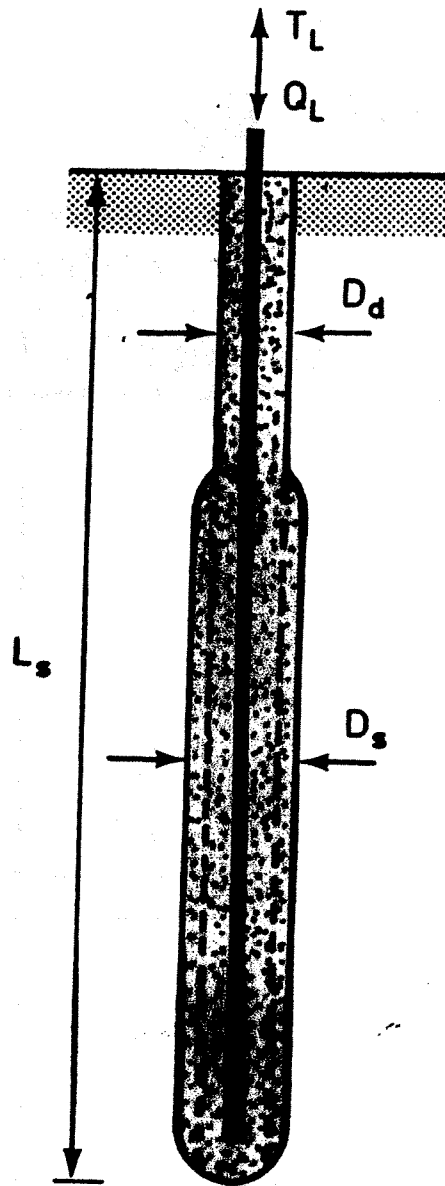
$(D_s = \alpha \cdot D_d)$

$q_s = f(p_\ell)$

CHARTS

**MICROPILE LOAD TESTS
ARE RECOMMENDED**

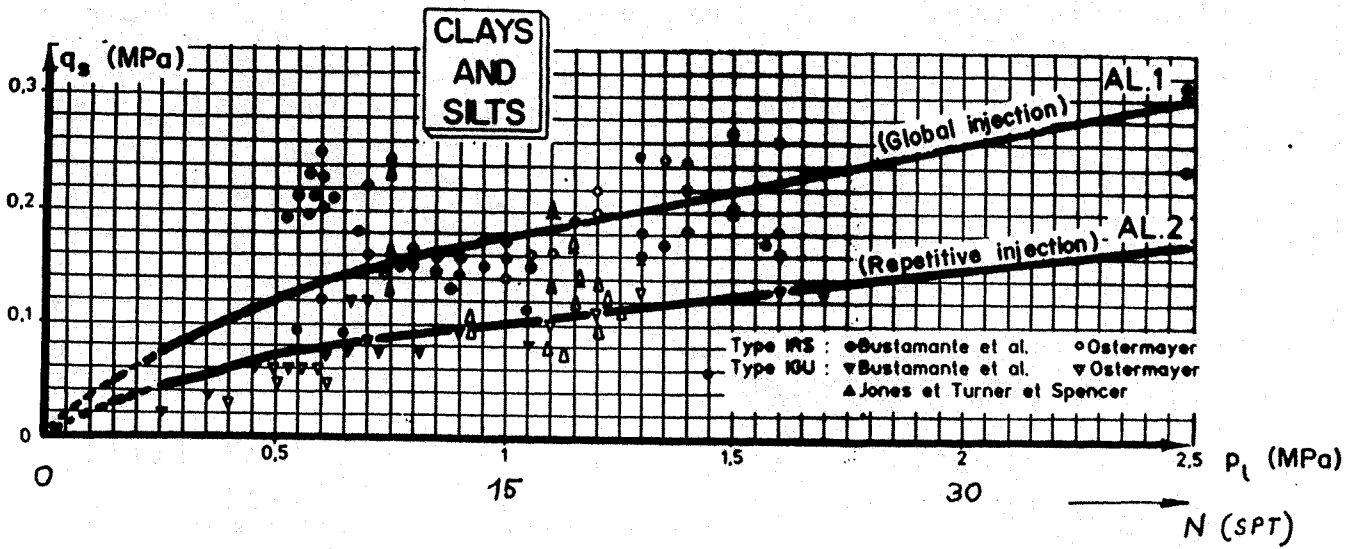
FS = 2

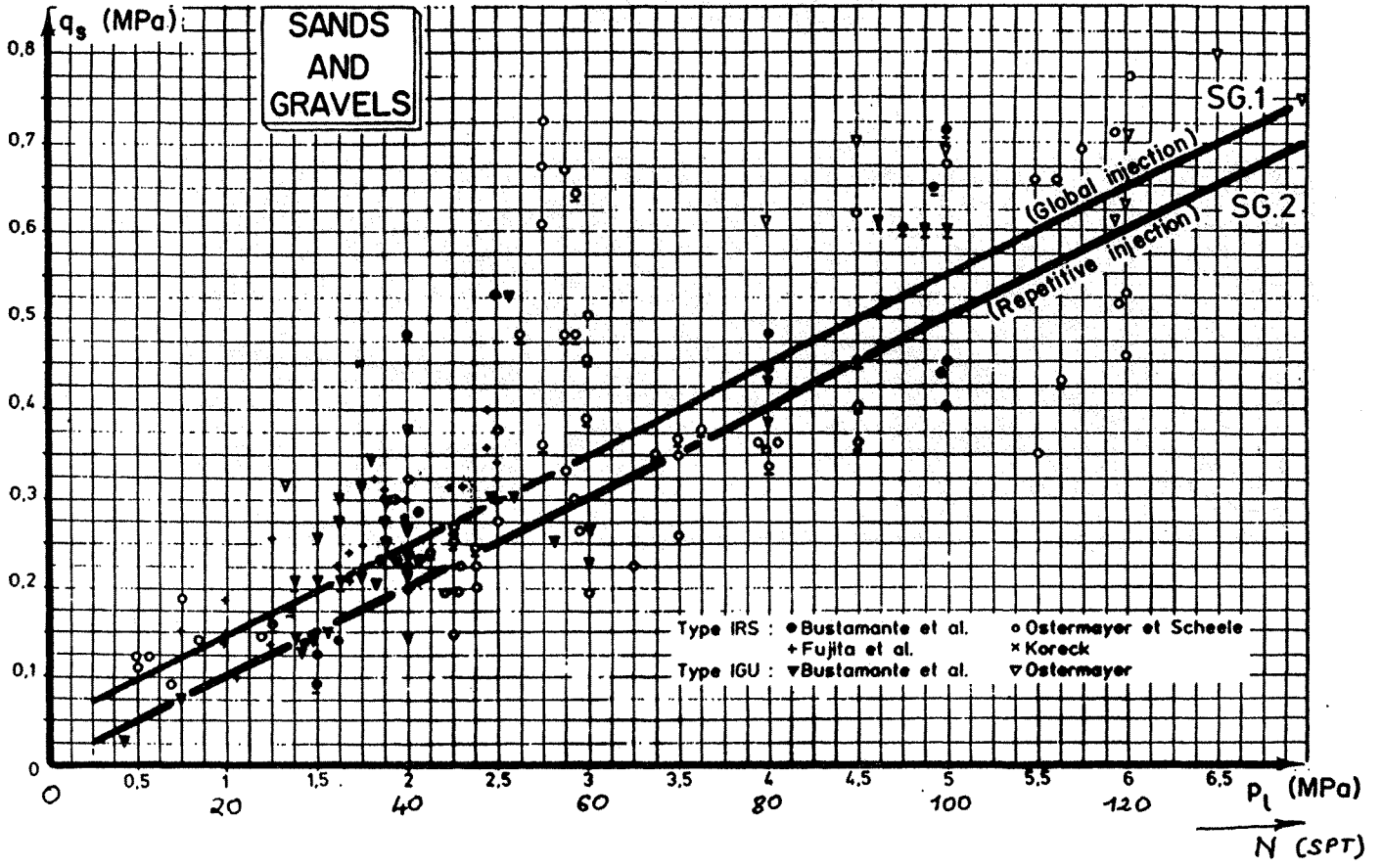


GEOMETRICAL FEATURES OF A MICROPILE

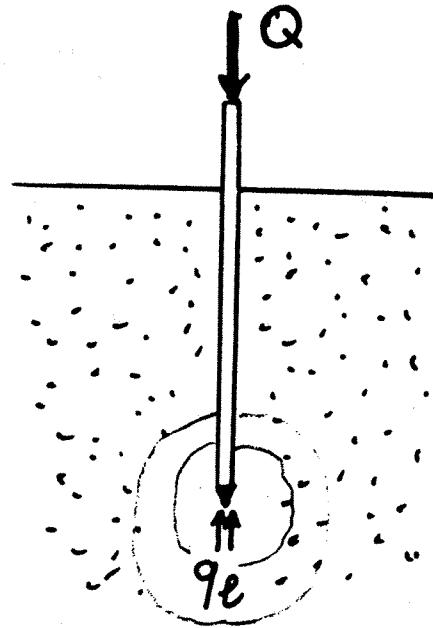
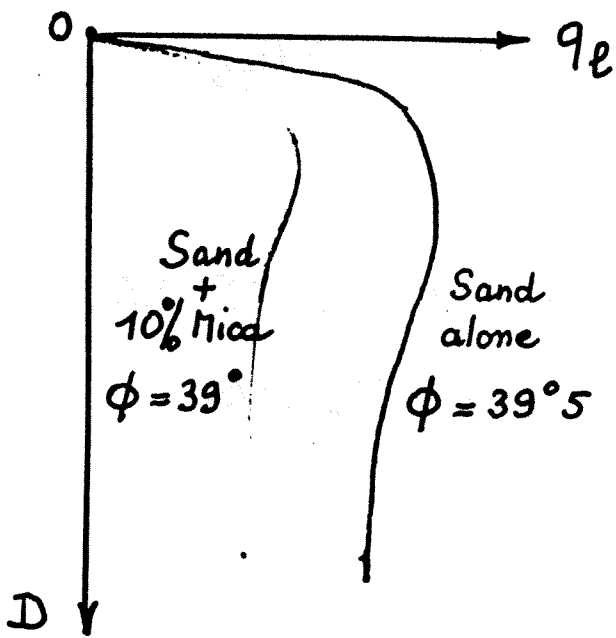
$$D_s = \alpha \cdot D_d$$

| SOILS | α Coefficient | |
|-----------------|----------------------|------------------|
| | Repetitive Injection | Global injection |
| Gravel | 1.8 | 1.3 to 1.4 |
| Sandy gravel | 1.6 to 1.8 | 1.2 to 1.4 |
| Gravelly sand | 1.5 to 1.6 | 1.2 to 1.3 |
| Coarse sand | 1.4 to 1.5 | 1.1 to 1.2 |
| Medium sand | 1.4 to 1.5 | 1.1 to 1.2 |
| Fine sand | 1.4 to 1.5 | 1.1 to 1.2 |
| Silty sand | 1.4 to 1.2 | 1.1 to 1.2 |
| Silt | 1.4 to 1.6 | 1.1 to 1.2 |
| Clay | 1.8 to 2 | 1.2 |
| Marl | 1.8 | 1.1 to 1.2 |
| Marly limestone | 1.8 | 1.1 to 1.2 |
| Chalk | 1.8 | 1.1 to 1.2 |
| Altered rock | 1.2 | 1.1 |





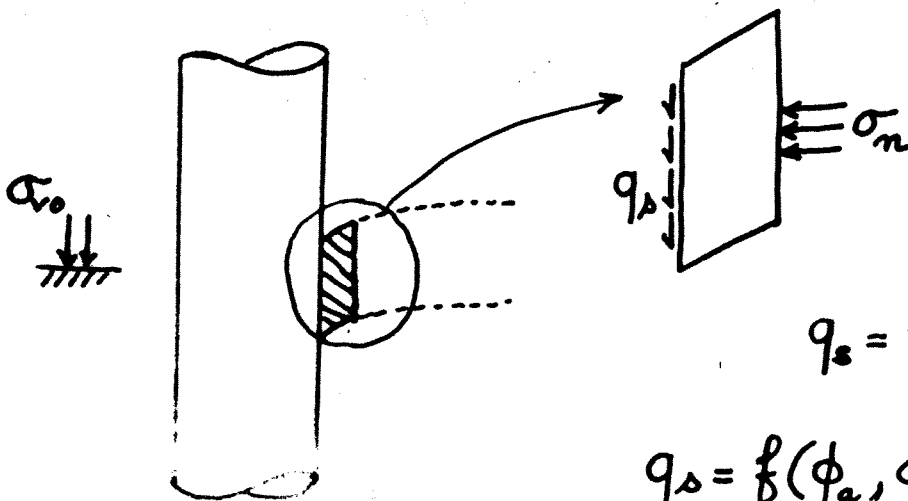
TIP RESISTANCE



$$q_e = f(\phi)$$

$$p_e \longleftrightarrow q_e = f(\phi, E, \dots)$$

FRICIONAL RESISTANCE



$$q_s = f(\phi_a) = \tan \phi_a \cdot K \cdot \sigma_z$$

$$q_s = f(\phi_a, \sigma_n, \Delta u, \dot{\epsilon}, \dots)$$

$$\updownarrow \Delta v$$

LIMIT STATE DESIGN

$$Q_u = Q_{pu} + Q_{su}$$

$$Q_{tu} = Q_{su}$$

$$Q_c = 0.5 Q_{pu} + 0.7 Q_{su}$$

$$Q_{tc} = 0.7 Q_{su}$$

1 ULTIMATE LIMIT STATE

- COMBINATIONS OF ACTIONS WITH LOAD FACTORS

_ FUNDAMENTAL

_ ACCIDENTAL

- Q_{pu}

$$Q_{su} = \sum Dd \cdot L_s \cdot q_s$$

$$\text{FUNDAMENTAL : } - \frac{Q_{tu}}{1.40} < Q < \frac{Q_u}{1.40}$$

$$\text{ACCIDENTAL : } - \frac{Q_{tu}}{1.20} < Q < \frac{Q_u}{1.20}$$

2 SERVICEABILITY STATE

- COMBINATIONS OF ACTIONS WITH LOAD FACTORS

_ RARE



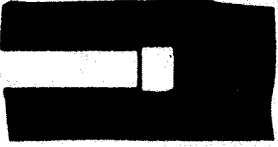

_ FREQUENT

_ QUASI - PERMANENT

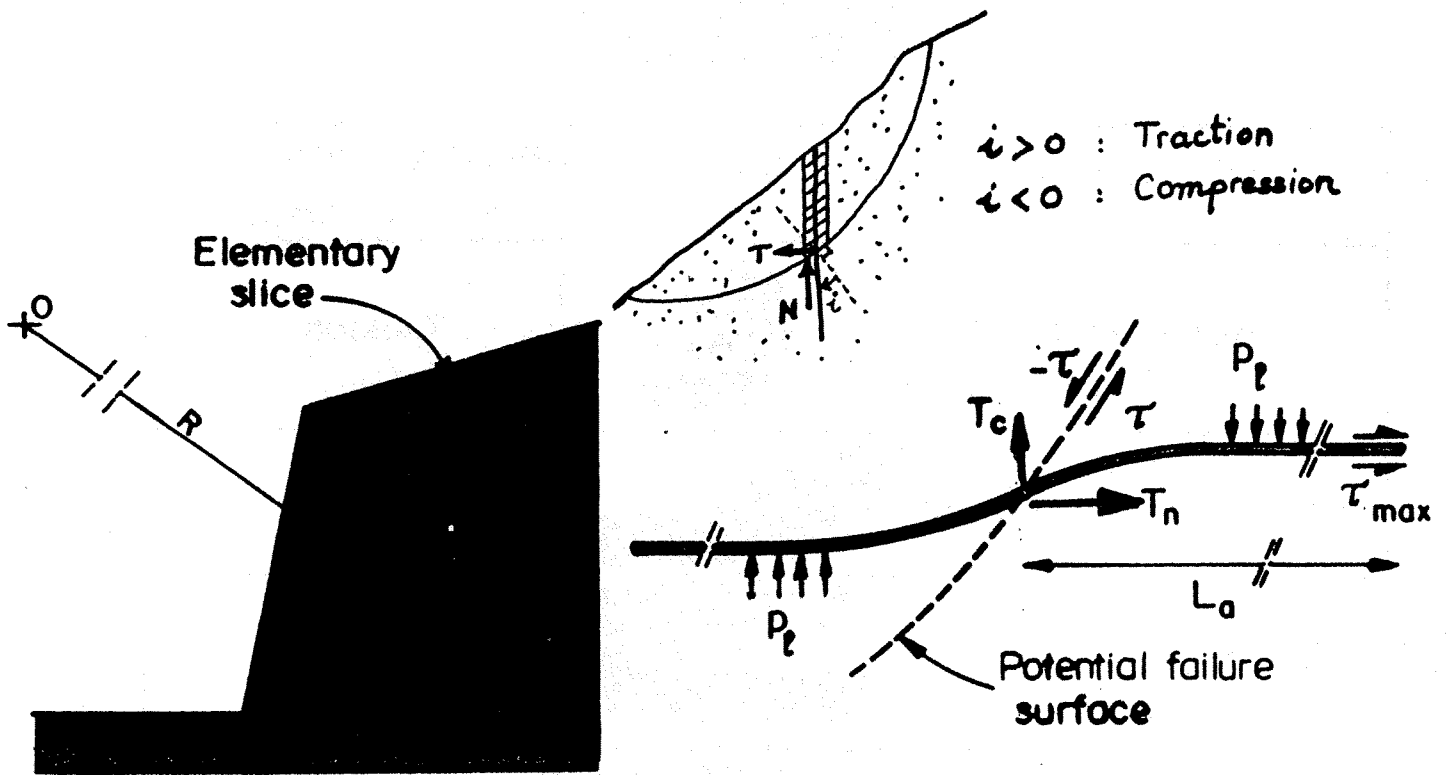
- $Q_c = 0.7 Q_{su}$

$$\text{RARE : } - \frac{Q_{tc}}{1.10} < Q < \frac{Q_c}{1.10}$$

$$\text{QUASI - PERMANENT : } - \frac{Q_{tc}}{1.40} < Q < \frac{Q_c}{1.40}$$

| TYPE OF STRUCTURE | PRIMARY FORCES IN THE NAILS |
|---|-----------------------------|
| ① Retaining structure  | Tension |
| ② Slope stabilization  | Bending |
| ③ Tunnels  | Tension |
| ④ Foundations  | Compression |

APPLICATION OF SOIL NAILING



PRINCIPLES OF TALREN STABILITY PROGRAM

| Sol n° | 19 | 19 | 19 | 20 |
|----------|------|------|------|------|
| γ | 1.05 | 1.05 | 1.05 | 1.05 |
| c | 0 | 0 | 0 | 20 |
| τ_u | 1.5 | 1.5 | 1.5 | 1.5 |
| Δ | 25 | 15 | 10 | 25 |
| τ_n | 1.2 | 1.2 | 1.2 | 1.2 |

Scale: 1/500
0 2 10

Units: kN meter and degree.
Calculation method: Perturbations

| | |
|----------------|-------|
| τ_{cal} | 13.82 |
| τ_{n1} | 1.02 |
| τ_{n2} | 1.01 |
| τ_{n3} | .98 |
| τ_{total} | 1 |
| τ_{ul} | 1 |
| τ_{total} | 1.5 |
| τ_{ul} | 1.355 |



TALREN 97
V1.0 of 18/09/97
TERRASOL

STABILIZING AN UNSTABLE SLOPE
WITH VERTICAL PILES
ULS CALCULATION
File: EXEMP17E.in

Proj: EXAMPL5

Study made by:
www.soc.

Figure:
8

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SOILS

| N° | γ | τ_{al} | c | $\Delta_0(z)$ | τ_0 | δ | τ_0 | r_u | q_u | pl | $K_{0.8}$ |
|----|----------|-------------|-----|---------------|----------|----------|----------|-------|-------|------|-----------|
| 1 | 19 | 1.05 | 0 | 0 | 1.5 | 25 | 1.2 | 0 | 0 | 0 | 0 |
| 2 | 19 | 1.05 | 0 | 0 | 1.5 | 15 | 1.2 | 0 | 0 | 0 | 0 |
| 3 | 19 | 1.05 | 0 | 0 | 1.5 | 10 | 1.2 | 0 | 0 | 0 | 0 |
| 4 | 20 | 1.05 | 20 | 0 | 1.5 | 25 | 1.2 | 0 | 0 | 0 | 0 |

NAILS

| N° | Yield st | Spacing | Elev. | Length | Inclin. | D bore | R shear | W plastic | Rigidity | Calc type |
|-----|----------|---------|-------|--------|---------|--------|---------|-----------|----------|-----------|
| Na1 | 0 | 2.4 | 22 | 16 | 90 | 2 | 340 | 0 | 0 | Tcal+Simp |
| Na2 | 0 | 2.4 | 21.75 | 16 | 90 | 2 | 340 | 0 | 0 | Tcal+Simp |
| Na3 | 0 | 2.4 | 21.5 | 16 | 90 | 2 | 340 | 0 | 0 | Tcal+Simp |

Unit weight of water : 10

Units : kN meter and degrees

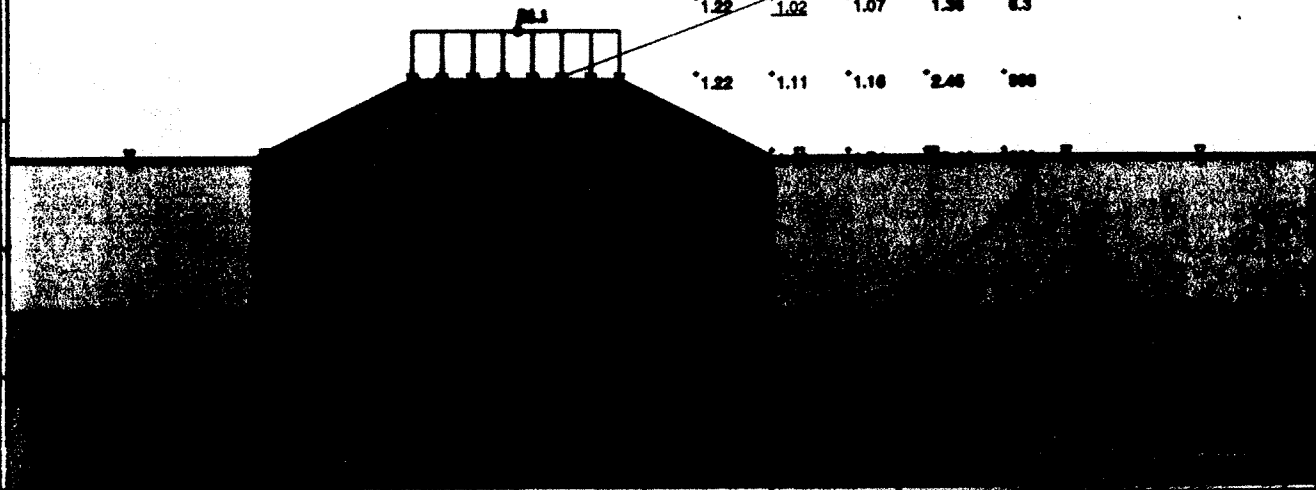
Calculation method : Perturbations

| Soil n° | 18 | 16 | 16.5 | 17 | 20 |
|--------------|------|-----|------|------|-------|
| γ | 1.05 | .95 | 1.05 | 1.05 | 1.05 |
| c | 0 | 6 | 12 | 20 | 0 |
| ϕ | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 |
| A | 30 | 0 | 10 | 10 | 35 |
| ϕ_a | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 |
| ϕ_{int} | 40 | 20 | 20 | 20 | 80 |
| p_1 | 400 | 40 | 80 | 140 | 800 |
| $K_{s.B}$ | 8800 | 180 | 200 | 240 | 17000 |

Units : kN meter and degrees.
Calculation method : Bishop.

| | |
|------------------|-------|
| γ_{total} | 1.02 |
| γ_{total} | 1.8 |
| γ_{int} | 1.9 |
| γ_{total} | 1.15 |
| γ_{int} | 1.125 |

| | | | | | |
|--|-------|-------|-------|-------|-------|
| | *1.62 | *1.19 | *1.08 | *1.11 | *1.47 |
| | *1.36 | *1.05 | *1.04 | *1.10 | *2.27 |
| | *1.22 | *1.02 | *1.07 | *1.36 | *6.3 |
| | *1.22 | *1.11 | *1.16 | *2.46 | *800 |



TALREN 97
V1.0 of 10/09/97
TERRASOL

EMBANKMENT REINFORCED WITH
SUB-VERTICAL MICROPILES
ULS CALCULATION
File: EXEMP18E.IN

Proj: EXAMPLIES

Study made by :
XXXXXXXXXX

Figure :
9

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SOILS

| N° | γ | γ_{s1} | c | ϕ (s) | ϕ_c | ϕ | ϕ' | r_u | q_u | p_1 | $K_{s.B}$ |
|----|----------|---------------|-----|------------|----------|--------|---------|-------|-------|-------|-----------|
| 1 | 18 | 1.05 | 0 | 0 | 1.5 | 30 | 1.2 | 0 | 40 | 400 | 8800 |
| 2 | 16 | .95 | 6 | 0 | 1.5 | 0 | 1.2 | 0 | 20 | 40 | 180 |
| 3 | 16.5 | 1.05 | 12 | 0 | 1.5 | 10 | 1.2 | 0 | 20 | 80 | 200 |
| 4 | 17 | 1.05 | 20 | 0 | 1.5 | 10 | 1.2 | 0 | 20 | 140 | 240 |
| 5 | 20 | 1.05 | 0 | 0 | 1.5 | 35 | 1.2 | 0 | 80 | 800 | 17000 |

DISTRIBUTED LOADS

| N° | σ_1 | σ_2 | γ_q |
|-----|------------|------------|------------|
| 8d1 | 20 | 20 | 1.3 |

NAILS

| N° | Yield σ_t | Spacing | Elev. | Length | Inclin. | D bore | R shear | M plastic | Rigidity | Calc type |
|-----|------------------|---------|-------|--------|---------|--------|---------|-----------|----------|-----------|
| Na1 | -2220 | 3 | 2 | 13 | 110 | .332 | -1110 | 183 | 7644 | Tcal+Sca1 |
| Na2 | -2220 | 3 | 2 | 13 | 95 | .166 | -1110 | 183 | 7644 | Tcal+Sca1 |
| Na3 | -2220 | 3 | 2 | 13 | 90 | .166 | -1110 | 183 | 7644 | Tcal+Sca1 |
| Na4 | -2220 | 3 | 2 | 13 | 85 | .166 | -1110 | 183 | 7644 | Tcal+Sca1 |
| Na5 | -2220 | 3 | 2 | 13 | 70 | .332 | -1110 | 183 | 7644 | Tcal+Sca1 |

Unit weight of water : 10
Units : kN meter and degrees
Calculation method : Bishop



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Projet National : Renforcement des sols par micropieux

RESEARCH PROGRAM

- **Basic problems**
- **Laboratory and centrifuge testing***
- **Experimental site at S^t Rémy***
- **Numerical modelling**

(*) plus slides

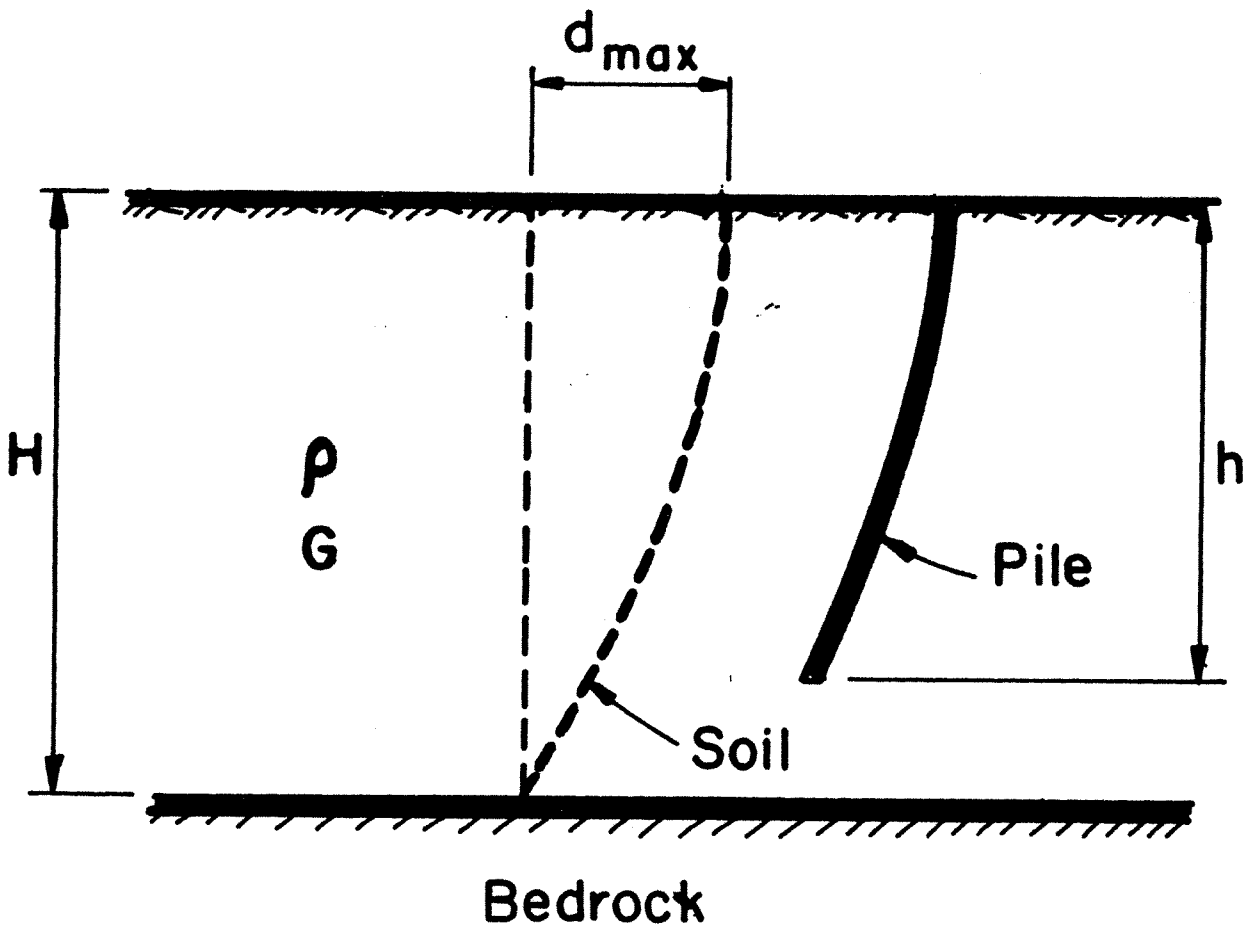
BASIC PROBLEMS OF MICROPILE GEOTECHNICAL STRUCTURES

- **Under axial loading**
- **Under lateral loading**
- **Buckling**
- **Seismic loading**
- **Corrosion**

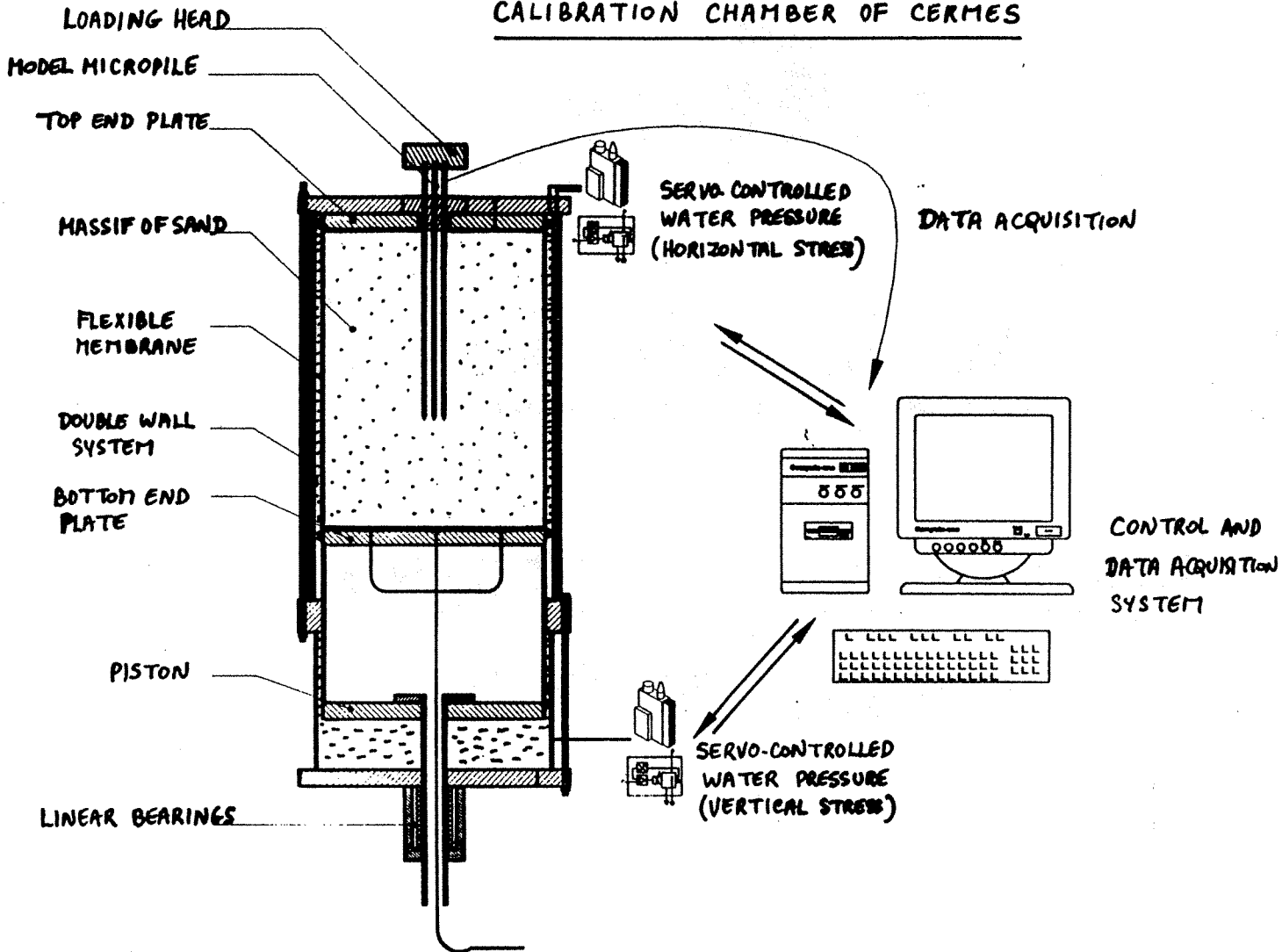
SEISMIC LOADING

Recommendations AFPS 90

Simplified approach

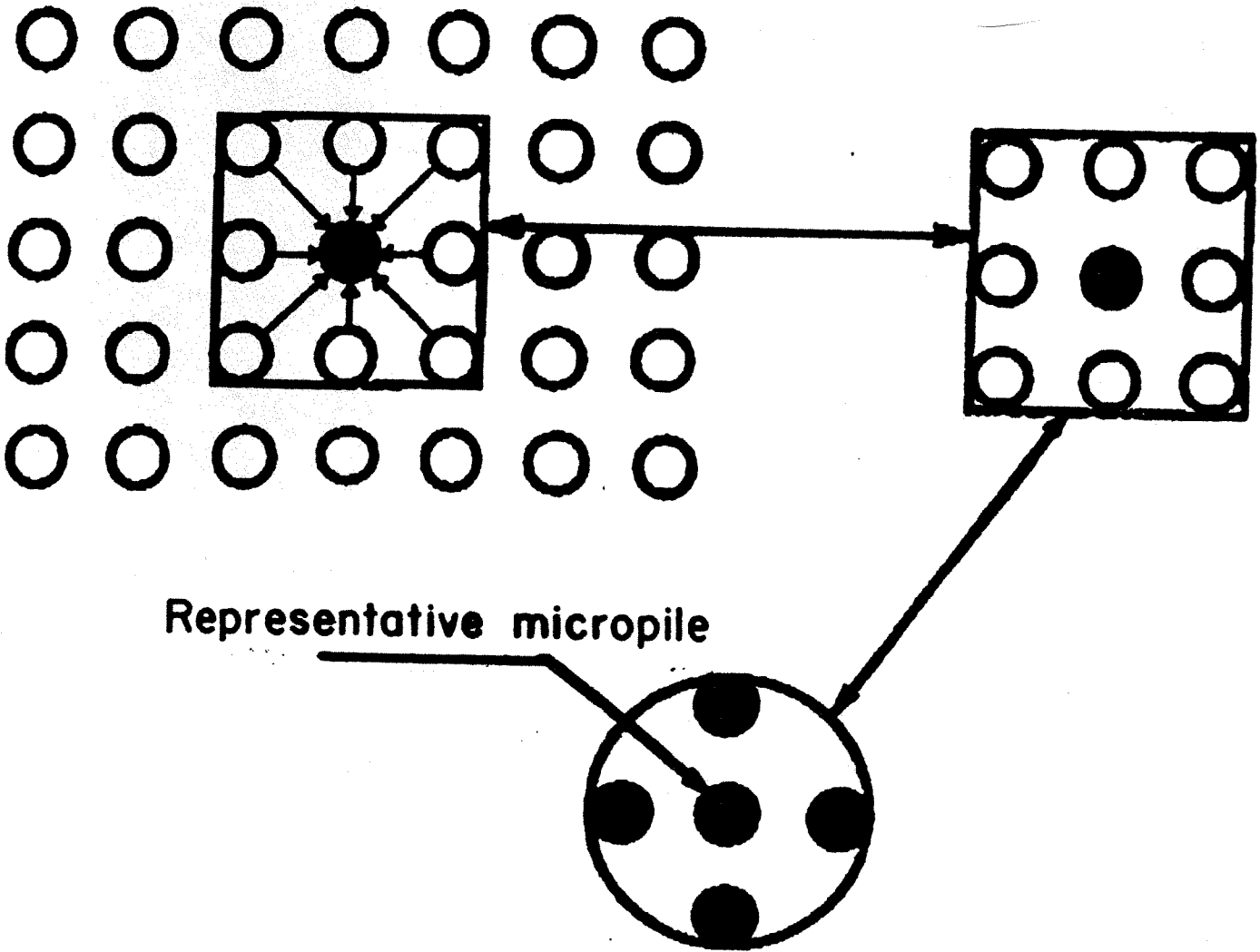


CALIBRATION CHAMBER OF CERMES



FOREVER

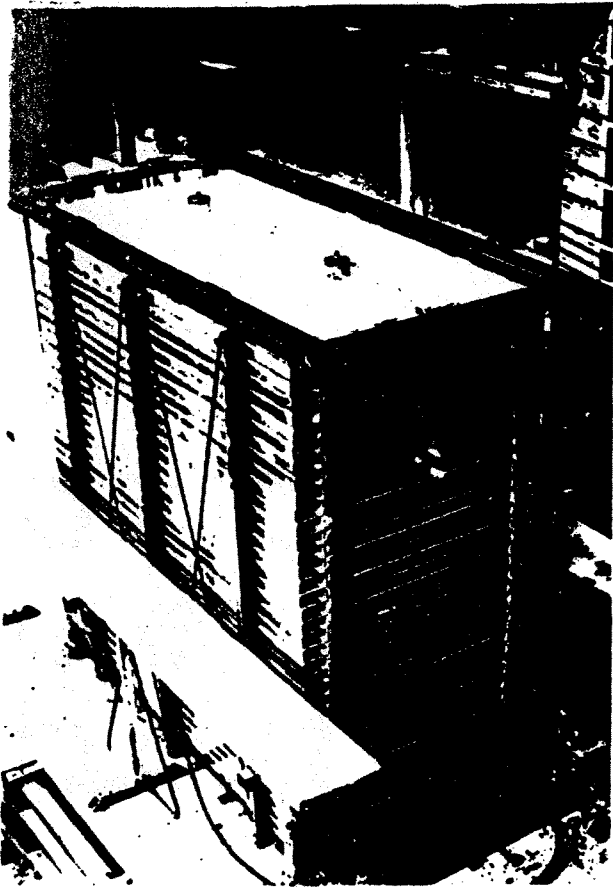
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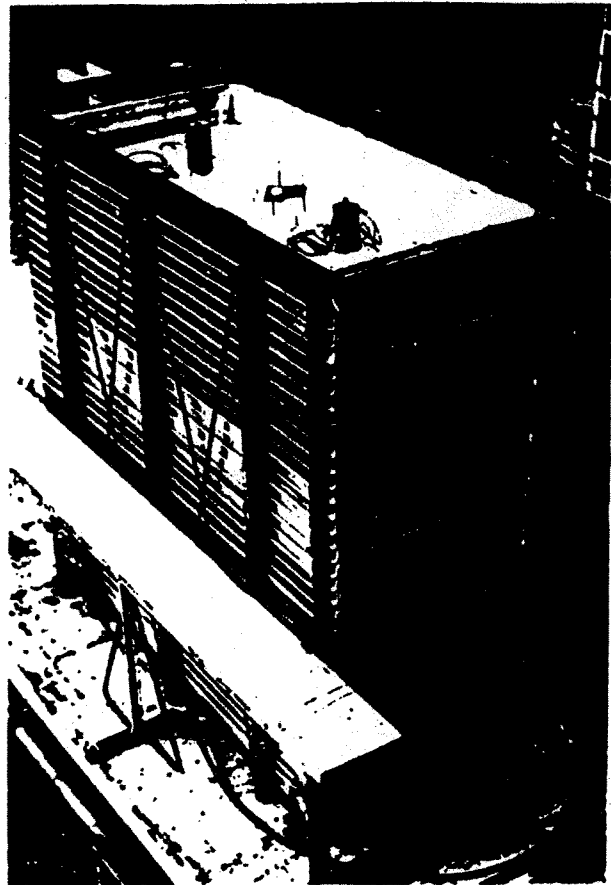
Representative micropile

BREAKDOWN OF A MICROPILE GROUP

UNIVERSITY OF CANTERBURY VIBRATING TABLE



Experimental set-up with two 95 mm diameter instrumented models before shaking



View of the set-up after very strong shaking



Dismounting of the set-up after testing

Seismic Behavior of Micropile Systems

OBJECTIVES

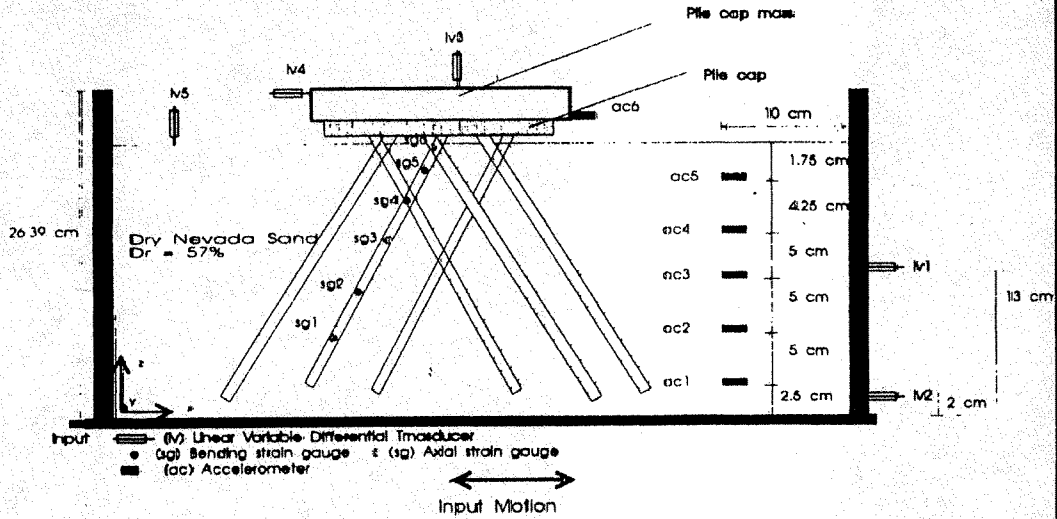
| PHASE | SOIL TYPE / MICROPILE SYSTEMS | ENGINEERING APPLICATIONS |
|-----------|--|--|
| Phase I | Loose Sand Micropile Groups | Foundation Underpinning Seismic Retrofitting |
| Phase II | Bi-layers and Silty Clays Micropile Groups | Foundation Underpinning Seismic Retrofitting |
| Phase III | Micropile Groups Micropile Networks | Prototype Systems Under Selected Range of Loading Conditions |
| Phase IV | Final Report Seismic Design Guidelines for Micropile Systems | Selected Engineering Applications Loading Conditions and Soil Types |

FOREVER - Cooperative Research Program

Soil Reinforcement

Test No 19
 Element : D=6.5 mm, L=21.3 cm, L/D=32.77
 Mcap= 0.491 kg
 failure load = 14 kg

s/D = 3
 a/g = 0.3
 Incln = -30 degrees



Typical Micropile Configuration
 Tested in the Centrifuge

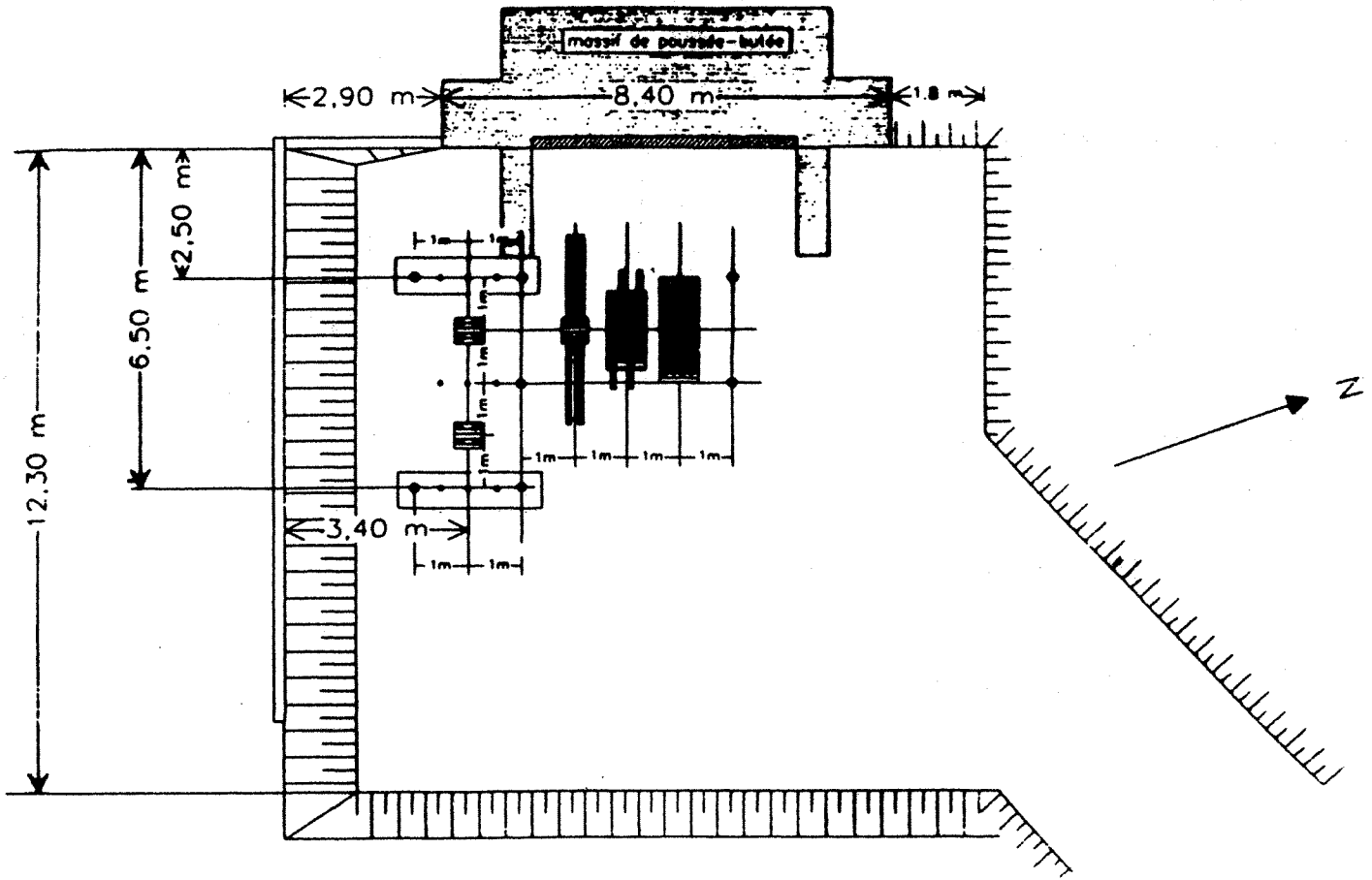
Hamburg, 97

**TESTING WITH THE LCPC CENTRIFUGE
AT NANTES**

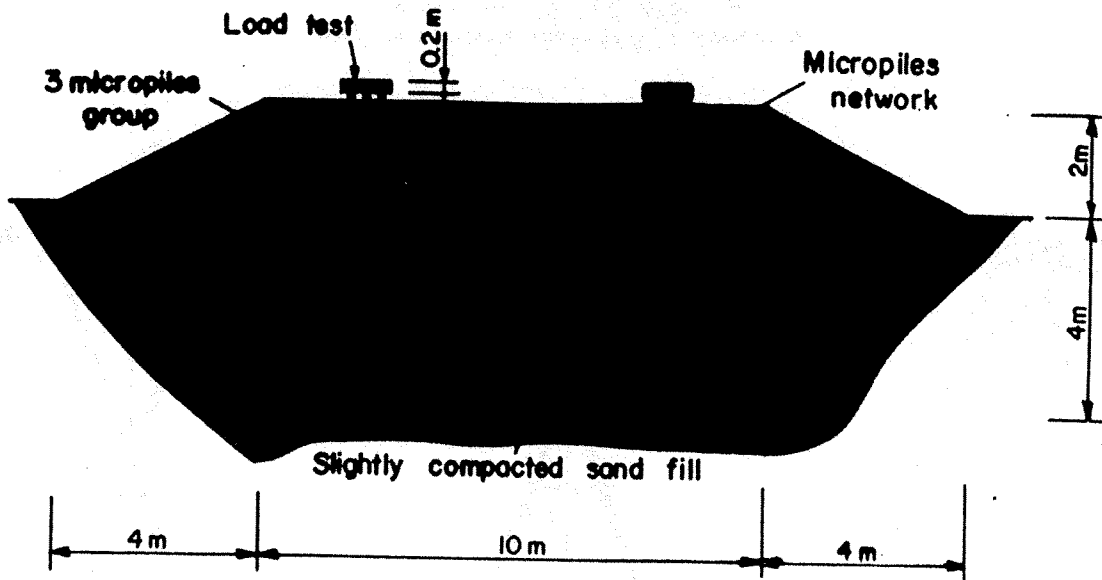
- **Buckling of micropiles**
- **Laterally loaded micropiles**
(p, y) experimental curves + comparison with PILATE
- **Groups of micropiles**
efficiency coefficients
 $\varnothing = 8\text{mm at } 40\text{g} \implies \varnothing = 32\text{ cm}$
- **Simple networks (pairs of micropiles)**

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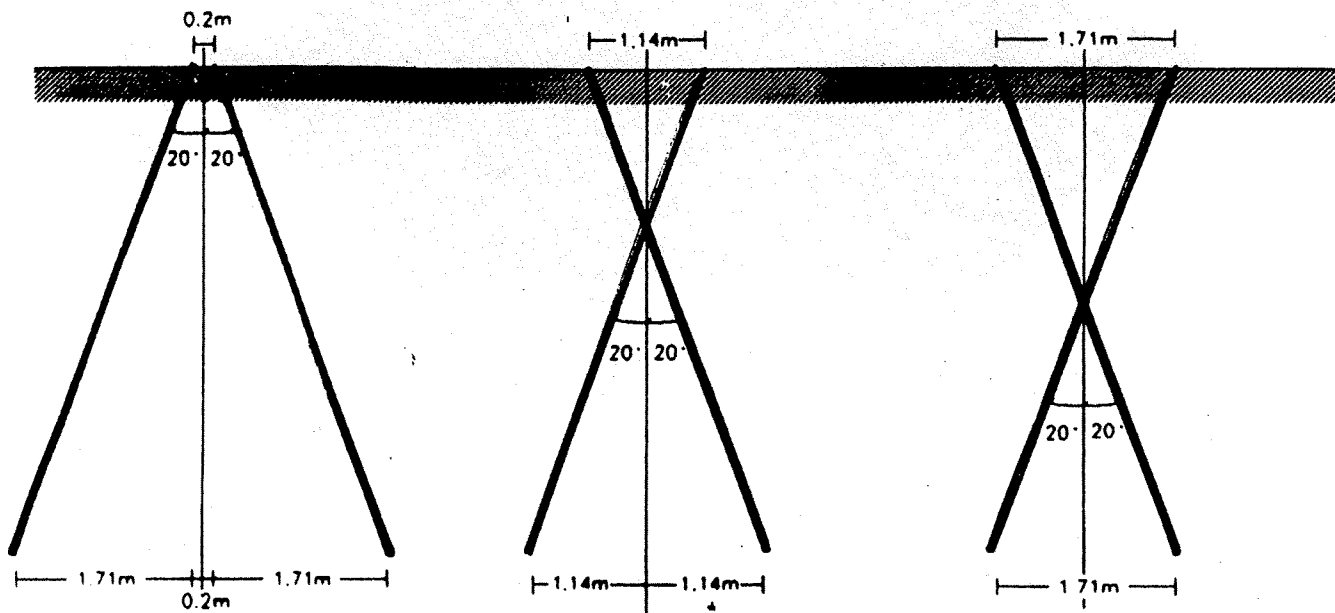
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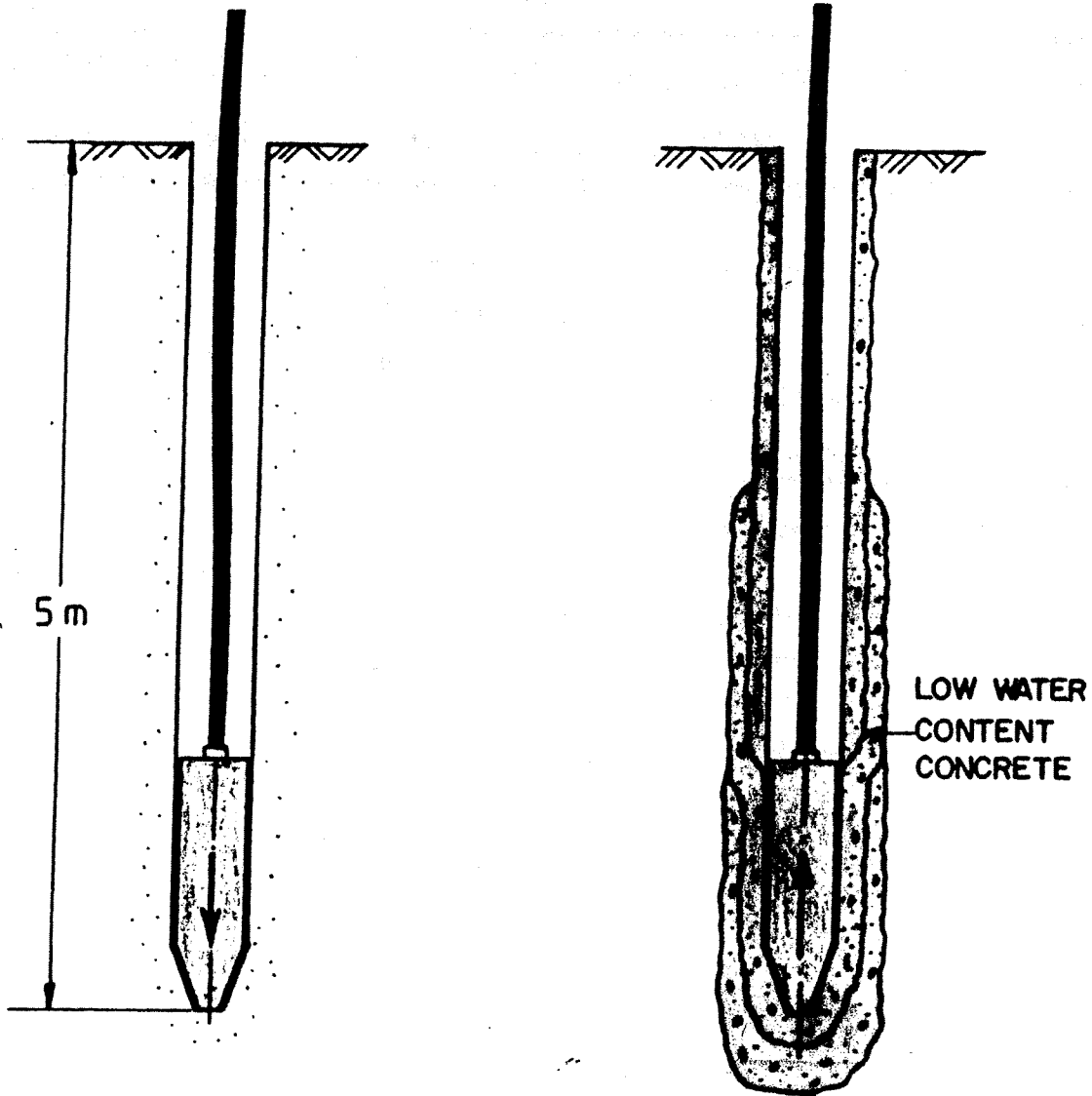
GENERAL ARRANGEMENT OF THE EXPERIMENTAL SITE
OF S^t REMY



FOREVER - MICROPILES
(Cross-section of the experimental site)



FULL SCALE TESTS ON SIMPLE NETWORKS AT S^t REMY



BORING BY SOIL DISPLACEMENT

**RAISING OF THE HAMMER
AFTER SEVERAL PASSES**

R-SOL TYPE MICROPILE

**NUMERICAL MODELLING OF GROUPS AND NETWORKS
OF MICROPILES WITH THE USE OF t - z AND p - y CURVES**

**Determination of t - z and p - y curves
Seismic soil displacement**

**ISOLATED
MICROPILES**

**Introduction of installation effects
Micropile - soil - micropile interaction
(efficiency coefficient)**

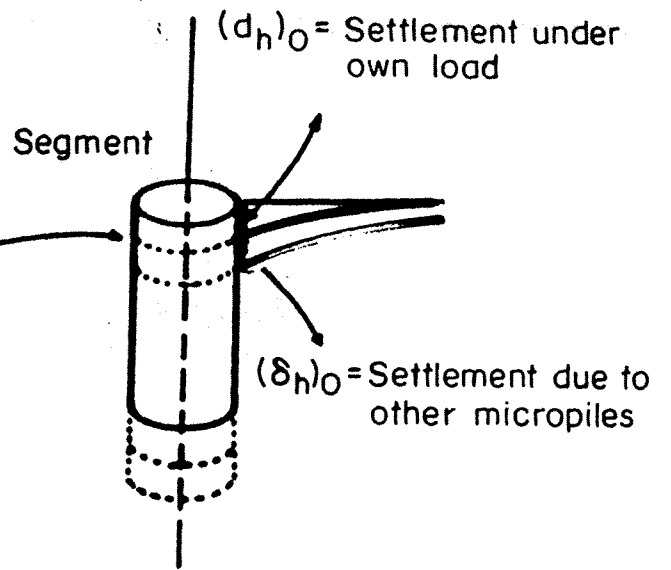
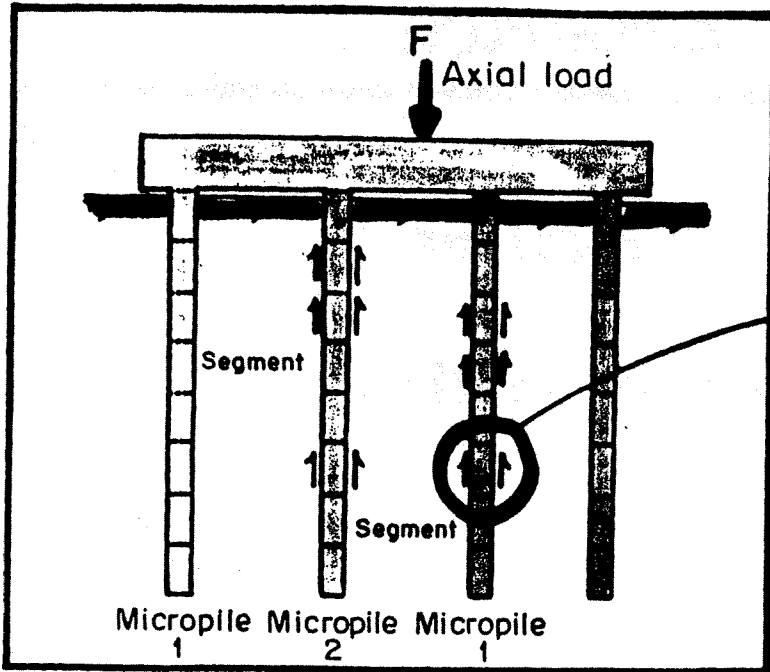
**GROUP OF
MICROPILES**

**Various raking angles of micropiles
Interlocking effects**

**NETWORKS OF
MICROPILES**

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**NUMERICAL MODELLING OF GROUPS AND
NETWORKS OF MICROPILES BY
CONTINUUM APPROACH**

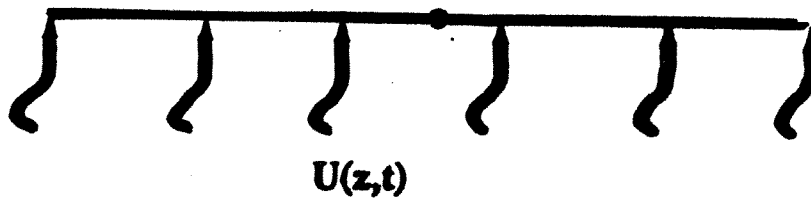
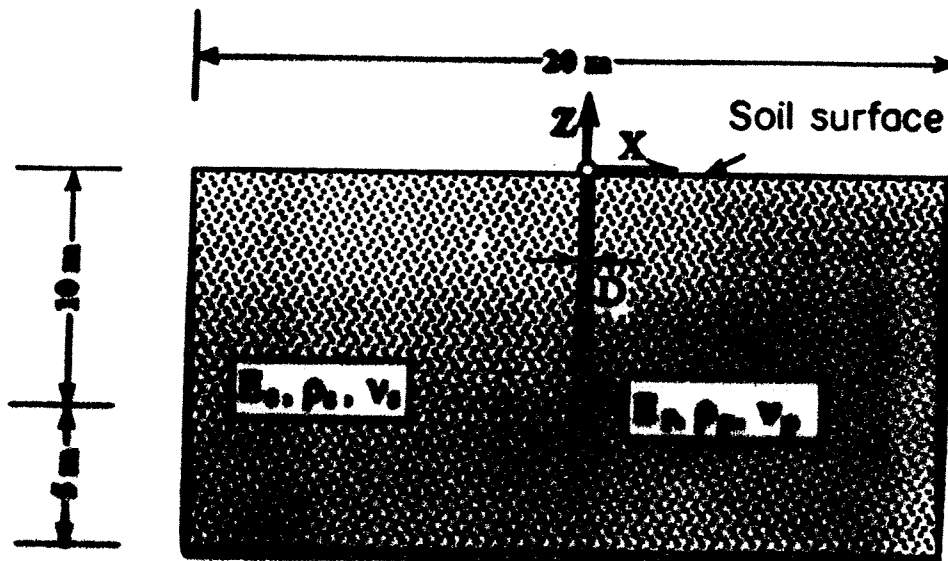
F.E.M calculations

Homogeneisation methods



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F.E.M. CALCULATION OF WAVE PROPAGATION IN A CONTINUUM CONTAINING A MICROPILE